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ATTORNEY DOCKET NUMBER

**TRANSMITTAL LETTER TO THE UNITED STATES
DESIGNATED/ELECTED OFFICE (DO/EO/US)
CONCERNING A FILING UNDER 35 U.S.C. 371**

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U.S. APPLICATION NO. (If known, see 37 CFR 1.5)

09/857482

INTERNATIONAL APPLICATION NO.
PCT/JP00/06898

INTERNATIONAL FILING DATE

PRIORITY DATE CLAIMED

TITLE OF INVENTION

DESIGN DEVICE OF CONTROLLER - UTILITY

APPLICANT(S) FOR DO/EO/US

Tatsuya Hojo; Atsushi Kurosaki

Applicant herewith submits to the United States Designated/Elected Office (DO/EO/US) the following items and other information:

1. ☒ This is a **FIRST** submission of items concerning a filing under 35 U.S.C. 371.
2. ☐ This is a **SECOND** or **SUBSEQUENT** submission of items concerning a filing under 35 U.S.C. 371.
3. ☒ This express request to begin national examination procedures (35 U.S.C. 371(f)) at any time rather than delay examination until the expiration of the applicable time limit set in 35 U.S.C. 371(b)) and PCT articles 22 and 39(1).
4. ☐ A proper Demand for International Preliminary Examination was made by the 19th month from the earliest claimed priority date.
5. ☒ A copy of the International Application as filed (35 U.S.C. 371(c)(2)).
 - a. ☒ is transmitted herewith (required only if not transmitted by the International Bureau).
 - b. ☐ has been transmitted by the International Bureau.
 - c. ☐ is not required, as the application was filed in the United States Receiving Office (RO/US).
6. ☒ A translation of the International Application into English (35 U.S.C. 371(c)(2)).
7. ☐ Amendments to the claims of the International Application under PCT Article 19 (35 U.S.C. 371(c)(3)).
 - a. ☐ is transmitted herewith (required only if not transmitted by the International Bureau).
 - b. ☐ have been transmitted by the International Bureau.
 - c. ☐ have not been made; however, the time limit for making such amendments has NOT expired.
 - d. ☐ have not been made and will not be made.
8. ☐ A translation of the amendments to the claims under PCT Article 19 (35 U.S.C. 371(c)(3)).
9. ☐ An oath or declaration of the inventor(s) (35 U.S.C. 371(c)(4)).
10. ☐ A translation of the annexes to the International Preliminary Examination Report under PCT Article 36 (35 U.S.C. 371(c)(5)).

Items 11. to 16. below concern document(s) or information included:

11. ☐ An Information Disclosure Statement under 37 CFR 1.97 and 1.98.
12. ☐ An assignment document for recording. A separate cover sheet in compliance with 37 CFR 3.28 and 3.31 is included.
13. ☐ A **FIRST** preliminary amendment.
☐ A **SECOND** or **SUBSEQUENT** preliminary amendment.
14. ☐ A subsequent specification.
15. ☐ A change of power of attorney and/or address letter.
16. ☐ Other items or information:

Specification and claims; Formal Drawings; Petition for PCT application; Notification of receipt of record copy; International Search Report; cited references; PCT publication no. W001/25861; Notice informing the applicant of the communication of the international application to the designated offices; Request for priority

Annex US.II, page 2 PCT Applicant's Guide - Volume II - National Chapter - US

U.S. APPLICATION NO (if known, see 37 CFR 1.5): 09/857482		INTERNATIONAL APPLICATION NO: PCT/JP00/06898		ATTORNEY'S DOCKET NUMBER: 96790P359	
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17. ☐ The following fees are submitted:

BASIC NATIONAL FEE (37 CFR 1.492 (a) (1) - (5)):

Neither international preliminary examination fee (37 CFR 1.482 nor international search fee (37 CFR 1.443(a)(2)) paid to USPTO and International Search Report not prepared by EPO or JPO **\$1000.00**

International preliminary examination fee (37CFR1.482)not paid to USPTO but International Search Report prepared by the EPO or JPO. **\$860.00**

International preliminary examination fee (37 CFR 1.482) not paid to USPTO but international search fee paid to USPTO (37 CFR 1.445(a)(2)) **\$700.00**

International preliminary examination fee paid to USPTO (37 CFR 1.482) but all claims did not satisfy provisions of PCT Article 33(1)-(4) **\$690.00**

International preliminary examination fee paid to USPTO (37 CFR 1.482) and all claims satisfied provisions of PCT Article 33(1)-(4) **\$100.00**

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Surcharge of **\$130.00** for furnishing the oath or declaration later than ☐ 20 ☐ 30 months from the earliest claimed priority date (37 CFR 1.492(e)).

CLAIMS	NUMBER FILED	NUMBER EXTRA	RATE		
Total claims	13 - 20 =	0	X \$18.00	\$	0.00
Independent claims	1 - 3 =	0	X \$78.00	\$	0.00
MULTIPLE DEPENDENT CLAIM(S) (if applicable)				+	\$270.00
TOTAL OF ABOVE CALCULATIONS =				\$	860.00
Reduction of 1/2 for filing by small entity, if applicable. Verified Small Entity Statement must also be filed (Note 37 CFR 1.9, 1.27, 1.28).				\$	
SUBTOTAL =				\$	860.00
Processing fee of \$130.00 for furnishing the English translation later than <input type="checkbox"/> 20 <input type="checkbox"/> 30 months from the earliest claimed priority date (37 CFR 1.492(f)).				+	\$
TOTAL NATIONAL FEE =				\$	860.00
Fee for recording the enclosed assignment (37 CFR 1.21(h)). The assignment must be accompanied by an appropriate cover sheet (37 CFR 3.28, 3.31). \$40.00 per property				+	\$
TOTAL FEES ENCLOSED =				\$	860.00
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a. ☒ A check in the amount of \$ 860.00 to cover the above fees is enclosed.

b. ☐ Please charge my Deposit Account No. _____ in the amount of \$ _____ to cover the above fees. A duplicate copy of this sheet is enclosed.

c. ☒ The Commissioner is hereby authorized to charge any additional fees which may be required, or credit any overpayment to Deposit Account No. 022666. A duplicate copy of this sheet is enclosed.

NOTE: Where an appropriate time limit under 37 CFR 1.495 has not been met, a petition to revive (37 CFR 1.137(a) or (b)) must be filed and granted to restore the application to pending status.

SEND ALL CORRESPONDENCE TO:

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SIGNATURE

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Our Ref. No.: 96790.P359
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UTILITY APPLICATION FOR UNITED STATES PATENT

FOR

DESIGN DEVICE OF CONTROLLER

Inventor(s): T. Hojo et al.

09/857482

11/PRTS

09/857482^{P14751-A}

JC18 Rec'd PCT/PTO 01 JUN 2001

Specification

Design Device of Controller

Technical Field

5 The present invention relates to a design device which designs a multivariable controller in accordance with H infinity ($H \infty$) logic.

Background Art

10 In recent years, in the feedback control field, the $H \infty$ logic has often been utilized which allows the design of a controller in view of an error between an actual control object and a numerical model of the control object. In the conventional control logic, when designing a control system, a control object model that is represented by the transfer
15 function and the state equation is prepared, and the control system is designed to stabilize the model. At this time, when there is an insignificant error between the actual control object and the model, a controller designed to stabilize the model can also stabilize the actual control object. However,
20 when there is a significant error between the actual control object and the model for some reason, the controller may not stabilize the actual control object.

25 In the $H \infty$ logic, even if there is an error between the actual control object and the numerical model for use with the design, when the information as to the error can be obtained, the controller for stabilizing the actual control object can be designed in view of the error. It is said that

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the H_{∞} logic is more likely to give the control specification intuitively in designing the control system, as compared with the conventional control logic. For example, in a case of designing a control system using the conventional control logic, its design specification involved a pole in the closed loop system or a weight matrix of evaluation function. However, the physical meanings of these values were unclear, and it required a lot of trial and error to make the settings.

On the contrary, in the H_{∞} logic, the control specification can be defined in accordance with the frequency responses of the closed loop system consisting of the control object and the controller. The H_{∞} logic has such an advantage, but is theoretically difficult, and has not been put into practical use in the current situation for the reasons of requiring the considerable knowledge to construct the actual control system, and it being difficult to give the control specification to the objects less treatable in accordance with the frequency responses in the process control and so forth.

20 Disclosure of the Invention

A control object model used in designing a multivariable control system has a variety of magnitudes of error components ranging from the manipulated variables to controlled variables. In this way, there are various error components of the model to the manipulated variables. In the H_{∞} logic, since the controller is designed with reference to the component with a large gain of error, the component with a

small gain of error is prone to have a very conservative response, or to be excessively stable. In some cases, it may be required to adjust the weight of control for each controlled variable to avoid the interference between
5 controlled variables. Thus, it is proposed to introduce a manipulated variable weight called a scaling matrix T in order to make the error magnitudes of the control object models consistent and weight the control for the controlled variables. However, in the conventional design method, no
10 general solution was not established to determine the scaling matrix T , resulting in the problem that the scaling matrix T was difficult to suitably choose. Since it was difficult to determine the scaling matrix T , there was another problem that the H_∞ logic was difficult to utilize in the design
15 of the multivariable controller.

Also, in the H_∞ logic, it is required to determine a frequency weight called a sensitivity weight W_s to determine the set value followup characteristic of the closed loop system. However, since the H_∞ logic is a design method in
20 the frequency domain, there was the problem that the design is easy in the control of the mechanical system, but is hard in the control system untreatable in the frequency domain such as the process control, whereby it is difficult to suitably select the sensitivity weight W_s . Also, since it is
25 difficult to give the control specification in the frequency domain, and hard to determine the sensitivity weight W_s , there was the problem that the H_∞ logic is difficult to utilize

in the design of the controller used in the process control field.

As described above, there was conventionally the problem that the H_{∞} logic was hard to utilize in the design of the controller.

The present invention has been made in order to solve these problems, and has as its object to provide a design device that can easily design a controller in accordance with the H_{∞} logic.

10 A design device of a controller according to the present invention comprises storage means for storing generalized plants, parameter calculating means for calculating the parameters of the components of the generalized plants in accordance with the response characteristic of a control
15 object model or the response characteristic of a closed loop system consisting of the control object model and the controller, and controller calculation means for calculating the parameters of the controller by applying the parameters to the generalized plants stored in the storage means.

20 In the design device of the controller according to one arrangement of the invention, the generalized plants have the control object models, and manipulated variable weight adjusting means for adjusting the input of manipulated variables into the control object models, which is provided
25 in the former stage of the control object models, the parameter calculating means comprises frequency response calculation means for calculating the frequency responses

of the control object models, and scaling matrix calculation means for calculating a scaling matrix T for determining the weighting of the manipulated variables with the manipulated variable weight adjusting means in accordance with the frequency responses of the control object models so that the respective gains of the control object models are consistent, and the controller calculation means calculates the parameters of the controller by applying the scaling matrix T to the manipulated variable weight adjusting means of the generalized plants stored in the storage means.

Also, in the design device of the controller according to one arrangement of the invention, the generalized plants have a first control object model for the manipulated variables, a second control object model for the disturbance, and manipulated variable weight adjusting means for adjusting the input of manipulated variables into the first control object model, which is provided in the former stage of the first control object model, the parameter calculating means comprises frequency response calculation means for calculating the frequency responses of the first control object model and the second control object model, and scaling matrix calculation means for calculating a scaling matrix T for determining the weighting of the manipulated variables with the manipulated variable weight adjusting means in accordance with the frequency responses of the first and second control object models so that the respective gains of the first control object model are consistent with the

maximum value of the gains of the second control object model,
and the controller calculation means calculates the
parameters of the controller by applying the scaling matrix
T to the manipulated variable weight adjusting means of the
5 generalized plants stored in the storage means.

Also, in the design device of the controller according
to one arrangement of the invention, the generalized plants
stored in the storage means have control variable weight
adjusting means for adjusting the controlled variables
10 inside a closed loop system consisting of the manipulated
variable weight adjusting means, the control object model
for the manipulated variables and the controller, and the
design device has setting means for setting a weight matrix
S for determining the weighting of the controlled variables
15 with the control variable weight adjusting means.

Also, in the design device of the controller according
to one arrangement of the invention, the generalized plants
stored in the storage means have control variable weight
adjusting means for adjusting the controlled variables in
20 the former or latter stage of frequency sensitivity weight
adjusting means to determine the set value followup
characteristic of a closed loop system consisting of the
manipulated variable weight adjusting means, the control
object models for the manipulated variables and the
25 controller, and the design device has setting means for
setting a weight matrix S for determining the weighting of
the controlled variables with the control variable weight

adjusting means.

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In the design device of the controller according to one arrangement of the invention, the parameter calculating means has setting means for setting the transient response
5 characteristic of the closed loop system and frequency sensitivity weight calculation means for calculating the frequency sensitivity weight to determine the set value followup characteristic of the closed loop system in accordance with the transient response characteristic of the
10 closed loop system, and the controller calculation means calculates the parameters of the controller by applying the frequency sensitivity weight to the generalized plants stored in the storage means.

In the design device of the controller according to one
15 arrangement of the invention, the frequency sensitivity weight calculation means calculates the frequency sensitivity weight in accordance with the transient response characteristic of the closed loop system, and a design index that the H_{∞} norm of a transfer function of the closed loop
20 system from the set value to the deviation, multiplied by the frequency sensitivity weight, is less than 1.

In the design device of the controller according to one arrangement of the invention, the setting means approximates the transient response characteristic of the closed loop
25 system with a first-order lag characteristic.

In the design device of the controller according to one arrangement of the invention, the setting means approximates

the transient response characteristic of the closed loop system with a second-order system characteristic.

Brief Description of the Drawings

Fig. 1 is a block diagram showing the configuration of a design device of a controller in a first embodiment of the present invention;

Fig. 2 is a block diagram showing the configuration of a model of an actual control object as represented in the formulae;

Fig. 3 is a block diagram showing the configuration of the conventional generalized plants;

Fig. 4 is a block diagram showing the configuration of the generalized plants for use with the design device of the invention;

Fig. 5 is a block diagram showing the configuration of a robust control system with a controller added to the generalized plants of Fig. 4;

Fig. 6 is a block diagram showing the configuration of an actual controller containing the controller designed using the design device in the first embodiment of the invention;

Fig. 7 is a block diagram showing an additive error in a numerical model of the control object;

Fig. 8 is a block diagram showing the configuration of a closed loop system used in determining the sensitivity weight;

Fig. 9 is a graph for explaining the operation of a

scaling matrix in the first embodiment of the invention;

Fig. 10 is a graph for explaining the operation of a scaling matrix in a second embodiment of the invention;

Fig. 11 is a block diagram showing the configuration of a design device of a controller in a third embodiment of the present invention;

Fig. 12 is a block diagram showing the configuration of the generalized plants in the third embodiment of the present invention;

Fig. 13 is a block diagram showing the configuration of an actual controller containing the controller designed using the design device in the third embodiment of the invention;

Fig. 14 is a block diagram showing the configuration of the generalized plants in a fourth embodiment of the present invention;

Fig. 15 is a block diagram showing the configuration of a design device of a controller in a fifth embodiment of the present invention;

Fig. 16 is a block diagram showing the configuration of a model of an actual control object as represented in the formulae;

Fig. 17 is a block diagram showing the configuration of the conventional generalized plants;

Fig. 18 is a block diagram showing the configuration of the generalized plants for use with the design device of the invention;

Fig. 19 is a block diagram showing the configuration of a robust control system with a controller added to the generalized plants of Fig. 18;

Fig. 20 is a block diagram showing the configuration of an actual controller containing the controller designed using the design device of the invention;

Fig. 21 is a block showing an additive error in a numerical model of the control object;

Fig. 22 is a block diagram showing the configuration of a closed loop system used in determining the sensitivity weight; and

Fig. 23 is a graph showing the time response characteristic when the closed loop system is approximated by a second-order system.

Best Mode of Carrying Out the Invention

First embodiment

The present invention will be described below in detail by way of embodiment with reference to the accompanying drawings. Fig. 1 is a block diagram showing the configuration of a design device of a controller in a first embodiment of the invention. The design device of Fig. 1 comprises a control object model input unit 1 for inputting the parameters of a control object model, a control object model registration unit 2 for registering the model parameters in a memory unit described later, the memory unit 3 for storing formulae of generalized plants and formulae of control object models which are parts of the generalized plants, a frequency

response calculation unit 4 for calculating the frequency responses of the control object models, a scaling matrix calculation unit 5 for calculating a scaling matrix T for making consistent the magnitudes of errors of the control object models so that the respective gains of the control object models are consistent with the maximum value of the gains of the control object models, and a controller calculation unit 6 for calculating the parameters of a controller by applying the scaling matrix T to the generalized plants stored in the memory unit 3.

An algorithm for designing the controller in accordance with the H_∞ logic is effected based on the generalized plants as represented using the control objects. Therefore, the generalized plants will be first described. Fig. 2 is a block diagram showing the configuration of a model of an actual control object as represented in the formulae. A numerical model of the control object as shown in Fig. 2 is composed of a first control object model 11 for the manipulated variable u and a second control object model 12 for the disturbance w. Reference sign P_u denotes a transfer function of the model 11 and reference sign P_w denotes a transfer function of the model 12. The models 11, 12 are obtained as a result of the model identification using the data obtained by a step response test for the actual control object. The controlled variable y that is the output of control object is a sum of the outputs from the models 11 and 12.

Fig. 3 shows the configuration of the conventional

generalized plants containing such numerical model of control object. The generalized plants involve providing a frequency weight called a sensitivity weight W_s used to determine the set value followup characteristic and a frequency weight called a complementary sensitivity weight W_t used to determine the robust stability, and introducing the set value r , and the outputs z_1 , z_2 in addition to the input (manipulated variable) u of control object, input (disturbance) w , and output (controlled variable) y , to realize both the set value followup characteristic and the robust stability as shown in Fig. 3. Deviation e ($=y-r$) is an observation quantity or the input into the controller (not shown). Reference numeral 13 denotes a block (frequency sensitivity weight adjusting means) representing the sensitivity weight W_s , and reference sign Z_1 denotes an output for effecting the evaluation of the set value followup characteristic. Also, reference numeral 14 denotes a block representing the complementary sensitivity weight W_t , and reference sign Z_2 denotes an output for effecting the evaluation of the robust stability.

Conventionally, in the generalized plants as shown in Fig. 3, the complementary sensitivity weight W_t is determined by estimating the uncertainty of the models on the basis of the numerical models of control objects, and the sensitivity weight W_s is determined by directly specifying the frequency characteristic in view of the followupability to the set value r , whereby the parameters of the controller are determined

through the γ iteration. However, since employing the generalized plant of Fig. 3, the controller is designed on the basis of a larger gain due to differences in the gains for the plant outputs of the manipulated variables, the
5 obtained controller is likely to be very conservative, or excessively stable. Also, since the set value followup characteristic and the disturbance response characteristic are usually reciprocal, it is preferred to design with the weight according to the purpose rather than with the same
10 weight. Further, in the generalized plants of Fig. 3 containing no integral element, some steady-state deviation arises. If the sensitivity weight W_s is provided with the integral characteristic, the controller can have the integral characteristic, but the generalized plants become
15 unstable, not leading to the normal H_∞ problem.

Therefore, in this embodiment, the generalized plants as shown in Fig. 4 are considered. In Fig. 4, reference sign M denotes a scaling matrix for adjusting the influence of disturbance w on the controlled variable y , reference sign
20 T denotes a scaling matrix for making the magnitude of error of the control object model consistent, and reference sign $\alpha^{-1}I$ denotes a weight for providing the controller with the integral characteristic to eliminate the steady-state deviation. Herein, $\alpha(s)$ is defined as $\alpha(s) = s/(s+a)$. Where
25 s is a Laplace operator, and a (>0) is any real number. Reference numeral 15 denotes a block representing the scaling matrix M, reference numeral 16 denotes a block (manipulated

variable weight adjusting means) representing the scaling matrix T , and reference numeral 17 denotes a block representing the weight $\alpha^{-1}I$. Deviation e_2 is deviation e multiplied by the weight $\alpha^{-1}I$, and input into the controller.

5 Fig. 5 shows the configuration of a robust control system in which a controller K is added to the above generalized plant. In Fig. 5, reference numeral 18 denotes a block representing the controller K .

The design device of the controller in this embodiment

10 is aimed at determining the parameters of the controller K such that the controlled variable y that is the output of control object follows the set value r , the influence of disturbance w is removed, and the control object is stabilized even if it is fluctuated or there is an error in the model

15 of control object. The H_∞ problem can be regarded as the problem of reducing the H_∞ norm (gain) of the transfer function from (r, w) to (z_1, z_2) . That is, the set value followup characteristic, the robust stability and the disturbance suppression may be considered in the following

20 way.

(A) Set value followup characteristic: If the H_∞ norm (gain) of the transfer function from the set value r to deviation e (more correctly, transfer function with the set value r multiplied by the frequency weight $\alpha^{-1}W_s$ from r to

25 z_1) is reduced, the deviation e can be decreased, so that the set value followup characteristic can be made better. Herein, $\alpha^{-1}W_s$ is the frequency weight for restricting the followup

band (e.g., followup only in the low band).

(B) Robust stability: There is an error between the actual control object and its model due to characteristic variations of the control object or the error at the time of modeling. The maximum value of the error from the identified model is estimated as $\Delta(s)$, and the controller K is designed such that the H_∞ norm from the set value r to z_2 is smaller than or equal to 1, employing the complementary sensitivity weight $W_t(s)$ such as

10 $|\Delta(j\omega)| < |W_t(j\omega)|$ for this error, whereby the robust stabilization can be achieved.

(C) Disturbance suppression: If the H_∞ norm (gain) of the transfer function from disturbance w to deviation e (more correctly, transfer function with the disturbance w

15 multiplied by the frequency weight $\alpha^{-1}W_s$ from w to z_1) is reduced, the deviation e can be decreased even if the disturbance w enters, whereby the disturbance suppression can be ameliorated.

Next, it is supposed that the state space representation

20 of the generalized plant as shown in Fig. 4 is given by:

$$\dot{x}_p = A_p x_p + B_{p1} M w + B_{p2} T u \quad \dots (1)$$

$$y = C_p x_p + D_{p1} M w + D_{p2} T u \quad \dots (2)$$

In the above expressions (1) and (2), x_p is the quantity

25 of state, and A_p , B_{p1} , B_{p2} , C_p , D_{p1} and D_{p2} are the parameters of the numerical models 11, 12 of control objects. From the

expression (2), the deviation e can be obtained in the following expression.

$$e = y - r = C_p x_p + D_{p1} M w + D_{p2} T u - r \quad \dots (3)$$

5 With the configuration of the generalized plant as shown in Fig. 4, the outputs z_1' and z_2' can be defined in the following expressions.

$$z_1' = e \quad \dots (4)$$

$$z_2' = u \quad \dots (5)$$

10

The frequency weight for providing the controller K with the integral characteristic can be defined in the following expression, using the expression (3).

$$\begin{aligned} \dot{x}_\alpha &= A_\alpha x_\alpha + B_\alpha e \\ &= A_\alpha x_\alpha + B_\alpha C_p x_p + B_\alpha D_{p1} M w + B_\alpha D_{p2} T u - B_\alpha r \quad \dots (6) \end{aligned}$$

15

$$\begin{aligned} e_2 &= C_\alpha x_\alpha + D_\alpha e \\ &= C_\alpha x_\alpha + D_\alpha C_p x_p + D_\alpha D_{p1} M w + D_\alpha D_{p2} T u - D_\alpha r \quad \dots (7) \end{aligned}$$

In the expressions (6) and (7), x_α is the quantity of state of $\alpha^{-1}I$, and A_α , B_α , C_α and D_α are the parameters of $\alpha^{-1}I$. Arranging the above expressions and representing them in a state space, the following three expressions can be obtained.

20

$$\frac{d}{dt} \begin{bmatrix} x_p \\ x_\alpha \end{bmatrix} = \begin{bmatrix} A_p & 0 \\ B_\alpha C_p & A_\alpha \end{bmatrix} \begin{bmatrix} x_p \\ x_\alpha \end{bmatrix} + \begin{bmatrix} 0 & B_{p1}M & B_{p2}T \\ -B_\alpha & B_\alpha D_{p1}M & B_\alpha D_{p2}T \end{bmatrix} \begin{bmatrix} r \\ w \\ u \end{bmatrix} \quad \dots (8)$$

$$\begin{bmatrix} z_1' \\ z_2 \end{bmatrix} = \begin{bmatrix} D_\alpha C_p & C_\alpha \\ 0 & 0 \end{bmatrix} \begin{bmatrix} x_p \\ x_\alpha \end{bmatrix} + \begin{bmatrix} -D_\alpha & D_\alpha D_{p1}M & D_\alpha D_{p2}T \\ 0 & 0 & I \end{bmatrix} \begin{bmatrix} r \\ w \\ u \end{bmatrix} \quad \dots (9)$$

$$e_2 = \begin{bmatrix} D_\alpha C_p & C_\alpha \end{bmatrix} \begin{bmatrix} x_p \\ x_\alpha \end{bmatrix} + \begin{bmatrix} -D_\alpha & D_\alpha D_{p1}M & D_\alpha D_{p2}T \end{bmatrix} \begin{bmatrix} r \\ w \\ u \end{bmatrix} \quad \dots (10)$$

Representing the expressions (8), (9) and (10) in
5 Doile's notation, the following expression can be obtained.

$$G(s) = \begin{bmatrix} A & B_1 & B_2 \\ C_1 & D_{11} & D_{12} \\ C_2 & D_{21} & D_{22} \end{bmatrix} \quad \dots (11)$$

Parameter A can be represented as follows:

$$A = \begin{bmatrix} A_p & 0 \\ B_\alpha C_p & A_\alpha \end{bmatrix} \quad \dots (12)$$

Parameters B₁ and B₂ can be represented as follows:

$$B_1 = \begin{bmatrix} 0 & B_{p1}M \\ -B_\alpha & B_\alpha D_{p1}M \end{bmatrix}, \quad B_2 = \begin{bmatrix} B_{p2}T \\ B_\alpha D_{p2}T \end{bmatrix} \quad \dots (13)$$

10

Also, parameters C₁ and C₂ can be represented as follows:

$$C_1 = \begin{bmatrix} D_\alpha C_p & C_\alpha \\ 0 & 0 \end{bmatrix}, \quad C_2 = \begin{bmatrix} D_\alpha C_p & C_\alpha \end{bmatrix} \quad \dots (14)$$

And the parameters D₁₁, D₁₂, D₂₁, D₂₂ can be represented
as follows:

$$D_{11} = \begin{bmatrix} -D_\alpha & D_\alpha D_{p1} M \\ 0 & 0 \end{bmatrix}, \quad D_{12} = \begin{bmatrix} D_\alpha D_{p2} T \\ I \end{bmatrix}$$

$$D_{21} = \begin{bmatrix} -D_\alpha & D_\alpha D_{p1} M \end{bmatrix}, \quad D_{22} = D_\alpha D_{p2} T \quad \dots (15)$$

The sensitivity weight W_s and the complementary sensitivity weight W_t are designed, and multiplied by the output parts of the expression (11). Through γ iteration, the controller K is obtained in the state space representation. Herein, the output parts of the expression (11) signify the parts corresponding to the outputs z_1' , z_2' in Fig. 4. Hence, an output equation of the parameters C_1 , D_{11} , D_{12} of the expression (11) may be multiplied by a diagonal matrix Q as represented in the following expression having the diagonal elements of sensitivity weight W_s and complementary sensitivity weight W_t from the left side. Thus, the parameters of the controller K can be calculated.

$$Q = \begin{bmatrix} W_s & 0 \\ 0 & W_t \end{bmatrix} \quad \dots (16)$$

The controller K is a solution of the H_∞ control problem with the generalized plants, and the actual controller mounted on the plants such as a distillation tower is the controller K multiplied by weight $\alpha^{-1}I$ and scaling matrix T , as shown in Fig. 6.

Next, a method for determining the complementary sensitivity weight W_t in this embodiment will be described below. The control object is varied in the characteristics, depending on the driving conditions. Normally, the control design is made based on a certain model, but in the robust

control design, the variation of control object and the magnitude of error of modeling are contained beforehand in the control design, and the controller is designed to be stable without much deterioration in the control performance even if there is any variation or error. Fig. 7 shows an additive error for the model 11 of control object. In Fig. 7, reference numeral 19 denotes a block representing the additive error Δ . In the robust control design, a variation in the characteristic of the control object owing to the driving conditions and a model error due to lower dimension of the model 11 are represented as the additive error Δ as shown in Fig. 7. If the characteristics of the control object are deviated from the model 11 due to this additive error Δ , the controller is designed such that the controller output may be stable. To this end, the complementary sensitivity weight W_t may be determined to cover the additive error Δ . The general expression of this complementary sensitivity weight W_t is shown in the following expression. Since the change of the model 12 is not related with the stability of the system, it is supposed that the model 11 alone is varied in designing the controller.

$$W_t = \begin{bmatrix} W_{t1} & 0 & 0 & \dots & 0 \\ 0 & W_{t2} & 0 & \dots & 0 \\ 0 & 0 & W_{t3} & \dots & 0 \\ \vdots & \vdots & \vdots & \ddots & \vdots \\ 0 & 0 & 0 & \dots & W_{tN} \end{bmatrix} \dots (17)$$

In this embodiment, for the additive error Δ with scaled magnitude, employing the scaling matrix T , the element of

the complementary sensitivity weight W_t is the maximum value G_{\max} of the gains of error Δ multiplied by a safety factor δ (δ is equal to 1, for example). Namely, the elements (weights) $W_{t1}, W_{t2}, W_{t3}, \dots, W_{tN}$ are defined as follows.

$$W_{t1} = W_{t2} = W_{t3} = W_{tN} = (1 + \delta) G_{\max} \quad \dots (18)$$

This embodiment is involved with the multivariable control system, and assuming that the number of manipulated variables u is N (N is a positive integer), the complementary sensitivity weight W_t is $N \times N$ matrix. Where W_{tN} is the weight for the N -th manipulated variable u_N .

Next, a method for determining the sensitivity weight W_s in this embodiment will be described below. First of all, a general expression of the sensitivity weight W_s is shown in the following expression.

$$W_s = \begin{bmatrix} W_{s1} & 0 & 0 & \dots & 0 \\ 0 & W_{s2} & 0 & \dots & 0 \\ 0 & 0 & W_{s3} & \dots & 0 \\ \vdots & \vdots & \vdots & \ddots & \vdots \\ 0 & 0 & 0 & \dots & W_{sL} \end{bmatrix} \quad \dots (19)$$

Assuming that the number of controlled variables y is L (L is a positive integer), the sensitivity weight W_s is $L \times L$ matrix. Element W_{sL} of the sensitivity weight W_s is the weight for the L -th controlled variable y_L . In order to determine the sensitivity weight W_s , a closed loop system of Fig. 8 in which the robust control system of Fig. 5 is simplified is considered. In Fig. 8, reference numeral 11a denotes a block representing a numerical model P of control object, and reference numeral 13a denotes a block representing the

frequency weight W_s' . Supposing that the sensitivity function indicating the control performance mainly regarding the quick-response property such as the set value

followupability or disturbance suppression is $S(s)$, the smaller gain $|S(j\omega)|$ of the sensitivity function $S(s)$ is preferable because the model variations have less effect on the set value response. If the control specification at each frequency is given by $S_{\text{spec}}(\omega)$, the following condition concerning the sensitivity function $S(s)$ can be obtained.

$$|S(j\omega)| < S_{\text{spec}}(\omega); \forall \omega \quad \dots (20)$$

Where $\forall \omega$ means that the expression (20) holds for all frequencies ω . Employing this sensitivity function $S(s)$, the design index of the controller K in view of the set value followup characteristic is as follows:

$$\|W_{sL}'(s)S(s)\|_{\infty} < 1 \quad \dots (21)$$

The frequency weight $W_{sL}'(s)$ is $W_{sL}(s)$ multiplied by $\alpha^{-1}(s)$, and is defined as follows:

$$W_{sL}'(s) = \alpha^{-1}(s)W_{sL}(s) \quad \dots (22)$$

The expression (21) indicates that the H_{∞} norm of the transfer function of the closed loop system of Fig. 8 from the set value r to the deviation e (more correctly, the transfer function with the set value r multiplied by the frequency weight $\alpha^{-1}(s)W_{sL}(s)$ from r to z_1) is less than 1. By setting the weight $W_{sL}(s)$ to satisfy this expression (21), the controller K can be designed in view of the set value followup characteristic.

Next, a method for determining the scaling matrix M will be described below. A general expression of the scaling matrix M is shown in the following expression.

$$M = \begin{bmatrix} M_1 & 0 & 0 & \dots & 0 \\ 0 & M_2 & 0 & \dots & 0 \\ 0 & 0 & M_3 & \dots & 0 \\ \vdots & \vdots & \vdots & \ddots & \vdots \\ 0 & 0 & 0 & \dots & M_J \end{bmatrix} \quad \dots (23)$$

5 Assuming that the number of disturbance w is J (J is a positive integer), the scaling matrix M is JxJ matrix. Element M_J of the scaling matrix M is the weight for the J-th disturbance w_J , with the initial value being 1. Each element M_J is an adjustment parameter for determining the disturbance suppression performance by adjusting the influence of each disturbance w_J on the controlled variable y. That is, when the suppression of the particular disturbance w is desired to be intensified, the element M_J concerning this disturbance w is made larger than 1.

15 Next, a method for determining the scaling matrix T in this embodiment will be described below. A general expression of the scaling matrix T is shown in the following expression.

$$T = \begin{bmatrix} T_1 & 0 & 0 & \dots & 0 \\ 0 & T_2 & 0 & \dots & 0 \\ 0 & 0 & T_3 & \dots & 0 \\ \vdots & \vdots & \vdots & \ddots & \vdots \\ 0 & 0 & 0 & \dots & T_N \end{bmatrix} \quad \dots (24)$$

20 Assuming that the number of manipulated variables u is N (N is a positive integer), the scaling matrix T is NxN matrix. Element T_N of the scaling matrix T is the weight for the N-th

manipulated variable u_N . Each element T_N is determined such that the magnitudes of the gains of the control object model 11 are as equal as possible. More specifically, each element T_N is determined as follows:

5

$$T_N = \frac{1}{L} \cdot \frac{\max(\|G_{y1u1}\|_\infty, \|G_{y1u2}\|_\infty, \dots, \|G_{y1uN}\|_\infty)}{\|G_{y1uN}\|_\infty} + \frac{1}{L} \cdot \frac{\max(\|G_{y2u1}\|_\infty, \|G_{y2u2}\|_\infty, \dots, \|G_{y2uN}\|_\infty)}{\|G_{y2uN}\|_\infty} + \dots + \frac{1}{L} \cdot \frac{\max(\|G_{yLu1}\|_\infty, \|G_{yLu2}\|_\infty, \dots, \|G_{yLuN}\|_\infty)}{\|G_{yLuN}\|_\infty} \quad \dots (25)$$

In the expression (25), G_{yLuN} is the transfer function of the control object model 11 of Fig. 4 from the N-th manipulated variable u_N to the L-th controlled variable y_L , and $\|G_{yLuN}\|_\infty$ is the H_∞ norm (gain) of the same transfer function. $\max(\|G_{yLu1}\|_\infty, \|G_{yLu2}\|_\infty, \dots, \|G_{yLuN}\|_\infty)$ means to select the maximum value from among the H_∞ norms $\|G_{yLu1}\|_\infty, \|G_{yLu2}\|_\infty, \dots$, and $\|G_{yLuN}\|_\infty$. To obtain the H_∞ norm $\|G_{yLuN}\|_\infty$, the model 11 as presented in the state equation representation may be transformed into the transfer function representation given by the following expression, and the gain of each frequency may be calculated from this transfer function.

15

$$\begin{bmatrix} y_1 \\ y_2 \\ y_3 \\ \vdots \\ y_L \end{bmatrix} = \begin{bmatrix} G_{y1u1} & G_{y1u2} & G_{y1u3} & \dots & G_{y1uN} \\ G_{y2u1} & G_{y2u2} & G_{y2u3} & \dots & G_{y2uN} \\ G_{y3u1} & G_{y3u2} & G_{y3u3} & \dots & G_{y3uN} \\ \vdots & \vdots & \vdots & \ddots & \vdots \\ G_{yLu1} & G_{yLu2} & G_{yLu3} & \dots & G_{yLuN} \end{bmatrix} \begin{bmatrix} u_1 \\ u_2 \\ u_3 \\ \vdots \\ u_N \end{bmatrix} \quad \dots (26)$$

Thereby, the H_∞ norm $\|G_{yLuN}\|_\infty$ can be obtained for each of the manipulated variables u and the controlled variables y , and the element T_N of the scaling matrix T can be obtained from the expression (25).

5 Referring now to Fig. 9, the operation of the scaling matrix T will be described below. Fig. 9A shows the gain characteristic of the control object model 11 (frequency response characteristic of the model 11). In Fig. 9, three sorts of gain characteristic are only shown to simplify the description, but if the number of manipulated variables u is N and the number of controlled variables y is L , $N \times L$ sorts of gains exist. As shown in Fig. 9A, in the case where there is no scaling matrix T , it will be found that the gains of the control object model 11 are inconsistent. In general, 10 if the gains of the control object model are inconsistent, the magnitudes of the errors of the control object model are correspondingly inconsistent. Since the complementary sensitivity weight W_t is determined to cover the additive error Δ , as previously described, it follows that the 15 controller is designed on the basis of the model with larger error, whereby the controller obtained is likely to be very conservative, or excessively stable.

Thus, the magnitudes of the gains are made consistent, employing the scaling matrix T . Fig. 9B shows the gain 25 characteristic of the control object model 11 in the case where the scaling matrix T of this embodiment is provided. $\|G_{y\max}\|_\infty$ is the maximum value of the gains of the model 11.

As will be clear from Fig. 9B, the method for determining the scaling matrix T of this embodiment as shown in the expressions (24) and (25) involves determining the scaling matrix T such that the gains are consistent with the gain maximum value $\|G_{y_{\max}}\|_{\infty}$ (more correctly, the approximation of the gain maximum value) of the model 11.

Referring now to Fig. 1, the above operation will be described below. The parameters of the control object model 11 are set in the control object model input unit 1 by the user of the design device. The control object model registration unit 2 registers the parameters input from the control object model input unit 1 into the formulae of the control object model stored beforehand in the memory unit 3. The control object model input unit 1 and the control object model registration unit 2 constitute model setting means for setting the control object model. The memory unit 3 stores the formulae of the generalized plants of Fig. 4 and the formulae of the control object models that are parts of the generalized plants, as described in the expressions (1) to (15). The frequency response calculation unit 4 transforms the model 11 as presented in the state equation representation which is registered in the memory unit 3 into the transfer function representation, and calculates the gain at each frequency from the transfer function. Subsequently, the scaling matrix calculation unit 5 calculates the scaling matrix T, employing the expressions (24) and (25), on the basis of the gains calculated in the frequency response

calculation unit 4, and outputs it to the controller
calculation unit 6. The controller calculation unit 6
registers the scaling matrix T in the formulae of the
generalized plants stored in the memory unit 3, and through
5 γ iteration, calculates the parameters of the controller K .
At this time, the complementary sensitivity weight W_t , the
sensitivity weight W_s and the scaling matrix M are preset in
the generalized plants in the memory unit 3. In this way,
the controller K can be designed.

10 As previously described, the conventional method has
no general way of determining the scaling matrix T , and
empirically determined the scaling matrix T . On the contrary,
in this embodiment, the scaling matrix T is calculated, in
accordance with the frequency responses of the control object
15 models 11, such that the respective gains of the control
object models are consistent with the gain maximum value (more
correctly, the approximation of the gain maximum value) of
the control object model 11. Hence, the scaling matrix T can
be easily determined. In this way, the multivariable
20 controller can be easily designed in accordance with the H
 ∞ logic which is superior in the set value followup
characteristic, and capable of stabilizing the controller
even when the control objects are varied or the control object
models 11 have some error. Consequently, the multivariable
25 control system can be easily designed in view of the
variations of the control objects and the uncertainty of the
numerical models. Also, the multivariable controller can be

realized utilizing the features of the H_∞ control with smaller computational load during execution of the control, and with which the small-scale control system can be implemented.

5 In this embodiment, the scaling matrix T is determined such that the respective gains of the control object models are consistent with the gain maximum value (more correctly, the approximation of the maximum value) of the control object model 11, but the scaling matrix T may be determined such
10 that the respective gains are consistent with the gain minimum value or gain average value of the control object model 11. To make the respective gains consistent with the gain minimum value (more correctly, the approximation of the minimum value), \max in the expression (25) may be replaced with \min
15 for selecting the minimum value of $\|G_{yLu1}\|_\infty$, $\|G_{yLu2}\|_\infty$, ..., and $\|G_{yLuN}\|_\infty$. And to make the respective gains consistent with the gain average value (more correctly, the approximation of the average value), \max in the expression (25) may be replaced with E for acquiring the average value of $\|G_{yLu1}\|_\infty$, $\|G_{yLu2}\|_\infty$,
20 ..., and $\|G_{yLuN}\|_\infty$.

Second embodiment

In the first embodiment, the disturbance w is not considered, but the control object model for the disturbance w may be obtained. Thus, in this second embodiment, a method
25 for determining the scaling matrix T in view of the influence of disturbance w in such a case will be described below. In this second embodiment, the general expression of the scaling

matrix T can be given by the expression (24) in the same manner as in the first embodiment.

And in this second embodiment, each element T_N of the scaling matrix T is determined in the following expression.

5

$$T_N = \frac{1}{L} \cdot \frac{\max(\|G_{y1w1}\|_\infty, \|G_{y1w2}\|_\infty, \dots, \|G_{y1wJ}\|_\infty)}{\|G_{y1uN}\|_\infty} \\ + \frac{1}{L} \cdot \frac{\max(\|G_{y2w1}\|_\infty, \|G_{y2w2}\|_\infty, \dots, \|G_{y2wJ}\|_\infty)}{\|G_{y2uN}\|_\infty} \\ + \dots + \frac{1}{L} \cdot \frac{\max(\|G_{yLw1}\|_\infty, \|G_{yLw2}\|_\infty, \dots, \|G_{yLwJ}\|_\infty)}{\|G_{yLuN}\|_\infty} \dots (27)$$

In the expression (27), G_{yLwJ} is the transfer function of the control object model 12 of Fig. 4 from the J-th disturbance w_J to the L-th controlled variable y_L , and $\|G_{yLwJ}\|_\infty$ is the H_∞ norm (gain) of the same transfer function. $\max(\|G_{yLw1}\|_\infty, \|G_{yLw2}\|_\infty, \dots, \|G_{yLwJ}\|_\infty)$ means to select the maximum value from the H_∞ norms $\|G_{yLw1}\|_\infty, \|G_{yLw2}\|_\infty, \dots$, and $\|G_{yLwJ}\|_\infty$. To obtain the H_∞ norm $\|G_{yLwJ}\|_\infty$, the model 12 as presented in the state equation representation may be transformed into the transfer function representation as in the following expression, and the gain of each frequency may be calculated from this transfer function.

$$\begin{bmatrix} y_{w1} \\ y_{w2} \\ y_{w3} \\ \vdots \\ y_{wL} \end{bmatrix} = \begin{bmatrix} G_{y1w1} & G_{y1w2} & G_{y1w3} & \cdots & G_{y1wJ} \\ G_{y2w1} & G_{y2w2} & G_{y2w3} & \cdots & G_{y2wJ} \\ G_{y3w1} & G_{y3w2} & G_{y3w3} & \cdots & G_{y3wJ} \\ \vdots & \vdots & \vdots & \ddots & \vdots \\ G_{yLw1} & G_{yLw2} & G_{yLw3} & \cdots & G_{yLwJ} \end{bmatrix} \begin{bmatrix} w_1 \\ w_2 \\ w_3 \\ \vdots \\ w_J \end{bmatrix} \quad \dots (28)$$

In the expression (28), y_{wL} is the output of the control object model 12 for the disturbance w . Thereby, the H_∞ norm $\|G_{yLwJ}\|_\infty$ can be obtained for each of the disturbance w and the controlled variables y , and the element T_N of the scaling matrix T can be obtained from the expression (27).

Referring now to Fig. 10, the operation of the scaling matrix T will be described below. Fig. 10A shows the gain characteristic of the control object model 12 (frequency response characteristic of the model 12). In Fig. 10A, three sorts of gain characteristic are only shown to simplify the description, but if the number of disturbance w is J and the number of controlled variables y is L , $J \times L$ sorts of gain exist. $\|G_{ywmax}\|_\infty$ is the maximum value of the gains of the model 12.

On the other hand, Fig. 10B shows the gain characteristic of the control object model 11. As shown in Fig. 10B, it will be found that the gain maximum value of the control object model 12 and the gains of the control object model 11 are inconsistent.

Fig. 10C shows the gain characteristic of the control object model 11 in the case where the scaling matrix T of this embodiment is provided. As will be clear from Fig. 10C, the method for determining the scaling matrix T of this embodiment as shown in the expressions (24) and (27) involves

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determining the scaling matrix T such that the respective gains of the model 11 are consistent with the gain maximum value $\|G_{y_{wmax}}\|_{\infty}$ (more correctly, the approximation of the gain maximum value) of the model 12.

5 The scaling matrix T for the manipulated variable u is included in the closed loop system in mounting the controller. Accordingly, there is a meaning in making the magnitudes of the gains of the model 11 consistent, and it is not necessarily of importance with which the gain from the manipulated
10 variable u to the controlled variable y is consistent. The previous first embodiment illustrates one instance with which the respective gains of the control object models are consistent. On the contrary, in this second embodiment, because the input of disturbance is considered, it is
15 necessary that the influence of the input disturbance w is suppressed by the manipulated variable u from the viewpoint of suppressing the disturbance w . Thus, in this second embodiment, to cope with the worst situation, the scaling matrix T is determined such that the gains of the model 11
20 are consistent with the gain maximum value $\|G_{y_{wmax}}\|_{\infty}$ (more correctly, the approximation of the gain maximum value) of the model 12.

25 In this second embodiment, the configuration of the design device is almost equivalent to that of the first embodiment. Thus, the operation of the design device of this second embodiment will be described below with reference to Fig. 1.

The parameters of the control object model (model 11, 12 in this second embodiment) are set in the control object model input unit 1 by the user of the design device. The control object model registration unit 2 registers the parameters input from the control object model input unit 1 into the formulae of the control object model stored beforehand in the memory unit 3. The frequency response calculation unit 3 transforms the model 11, 12 as presented in the state equation representation which is registered in the memory unit 3 into the transfer function representation, and calculates the gain at each frequency from the transfer function. Subsequently, the scaling matrix calculation unit 5 calculates the scaling matrix T , employing the expressions (24) and (27), on the basis of the gain calculated in the frequency response calculation unit 4, and outputs it to the controller calculation unit 6. The operation of the controller calculation unit 6 is exactly the same as in the first embodiment. In this way, the controller K can be designed.

As described above, in this second embodiment, the scaling matrix T is calculated, on the basis of the frequency response of the first and second control object models 11, 12, such that the respective gains of the first control object model 11 are consistent with the maximum value of the gains of the second control object model 12. Hence, the scaling matrix T can be easily determined. Thereby, the multivariable controller can be easily designed in accordance with the H

∞ logic which is superior in the set value followup characteristic and disturbance suppression, and capable of stabilizing even when the control object is varied or the control object model has some error.

5 Third embodiment

In the first and second embodiments, the magnitudes of the gains of the model are made consistent by the scaling matrix T, so that the weights of control for the controlled variables are even. However, in practice, there is the problem
10 that the controlled variables y interfere with each other in the control, and the control is unstable, whereby it may be sometimes required to coordinate the weights of control for the controlled variables. Thus, in this second embodiment, a weight matrix S is introduced to weight the controlled
15 variables y directly.

Fig. 11 is a block diagram showing the configuration of a design device of a controller in a third embodiment of the present invention. Fig. 12 is a block diagram showing the configuration of the generalized plant in this third
20 embodiment. The design device of Fig. 11 is the design device of the first or second embodiment as shown in Fig. 1, comprising additionally a control variable weight input unit 7 for inputting the weight for the controlled variable y, a control variable weight registration unit 8 for registering
25 the control variable weight in the device, and a weight matrix calculation unit 9 for calculating the weight matrix S based on the control variable weight. Also, the generalized plant

of Fig. 12 is the generalized plant of the first or second embodiment as shown in Fig. 4, with a block (control variable weight adjusting means) 20 representing the weight matrix S. In this embodiment, the control variable weight adjusting means 20 (weight matrix S) is provided inside a closed loop system composed of the manipulated variable weight adjusting means 16 (scaling matrix T), the control object model 11 and the controller K. A general expression of the weight matrix S is shown in the following expression.

$$S = \begin{bmatrix} S_1 & 0 & 0 & \dots & 0 \\ 0 & S_2 & 0 & \dots & 0 \\ 0 & 0 & S_3 & \dots & 0 \\ \vdots & \vdots & \vdots & \ddots & \vdots \\ 0 & 0 & 0 & \dots & S_L \end{bmatrix} \quad \dots (29)$$

Assuming that the number of controlled variables y is L (L is a positive integer), the weight matrix S is LxL matrix. Element S_L of the weight matrix S is the weight for the L-th controlled variable y_L. Each element S_L is determined in the following expression.

$$S_L = \frac{W_{yL}}{\max(W_{y1}, W_{y2}, \dots, W_{yL})} \quad \dots (30)$$

In the expression (30), W_{yL} is the control variable weight for the L-th controlled variable y_L. In this way, each controlled variable can be directly weighted by the weight matrix S.

Next, in this third embodiment, the configuration of

the generalized plant is modified as shown in Fig. 12, so that the following expression can hold.

$$e_1 = S e \quad \dots (31)$$

From the expressions (31) and (3), the expressions (6) and (7) can be rewritten in the following expression.

$$\begin{aligned} x_\alpha &= A_\alpha x_\alpha + B_\alpha e_1 \\ &= A_\alpha x_\alpha + B_\alpha S C_p x_p + B_\alpha S D_{p1} M w + B_\alpha S D_{p2} T u - B_\alpha S r \end{aligned} \quad \dots (32)$$

$$\begin{aligned} e_2 &= C_\alpha x_\alpha + D_\alpha e \\ &= C_\alpha x_\alpha + D_\alpha S C_p x_p + D_\alpha S D_{p1} M w + D_\alpha S D_{p2} T u - D_\alpha S r \end{aligned} \quad \dots (33)$$

Thereby, the expressions (8), (9) and (10) can be rewritten in the following expression.

$$\frac{d}{dt} \begin{bmatrix} x_p \\ x_\alpha \end{bmatrix} = \begin{bmatrix} A_p & 0 \\ B_\alpha S C_p & A_\alpha \end{bmatrix} \begin{bmatrix} x_p \\ x_\alpha \end{bmatrix} + \begin{bmatrix} 0 & B_{p1} M & B_{p2} T \\ -B_\alpha S & B_\alpha S D_{p1} M & B_\alpha S D_{p2} T \end{bmatrix} \begin{bmatrix} r \\ w \\ u \end{bmatrix} \quad \dots (34)$$

$$\begin{bmatrix} z_1' \\ z_2 \end{bmatrix} = \begin{bmatrix} D_\alpha S C_p & C_\alpha \\ 0 & 0 \end{bmatrix} \begin{bmatrix} x_p \\ x_\alpha \end{bmatrix} + \begin{bmatrix} -D_\alpha S & D_\alpha S D_{p1} M & D_\alpha S D_{p2} T \\ 0 & 0 & I \end{bmatrix} \begin{bmatrix} r \\ w \\ u \end{bmatrix} \quad \dots (35)$$

$$e_2 = \begin{bmatrix} D_\alpha S C_p & C_\alpha \end{bmatrix} \begin{bmatrix} x_p \\ x_\alpha \end{bmatrix} + \begin{bmatrix} -D_\alpha S & D_\alpha S D_{p1} M & D_\alpha S D_{p2} T \end{bmatrix} \begin{bmatrix} r \\ w \\ u \end{bmatrix} \quad \dots (36)$$

Representing the expressions (34), (35) and (36) in the Doile's notation as in the expression (11), the parameter

A in the expression (11) can be represented as follows:

$$A = \begin{bmatrix} A_p & 0 \\ B_\alpha S C_p & A_\alpha \end{bmatrix} \quad \dots (37)$$

The parameters B_1 and B_2 can be represented in the following expression.

$$B_1 = \begin{bmatrix} 0 & B_{p1}M \\ -B_\alpha S & B_\alpha S D_{p1}M \end{bmatrix}, \quad B_2 = \begin{bmatrix} B_{p2}T \\ B_\alpha S D_{p2}T \end{bmatrix} \quad \dots (38)$$

The parameters C_1 and C_2 can be represented in the following expression.

$$C_1 = \begin{bmatrix} D_\alpha S C_p & C_\alpha \\ 0 & 0 \end{bmatrix}, \quad C_2 = [D_\alpha S C_p \quad C_\alpha] \quad \dots (39)$$

The parameters D_{11} , D_{12} , D_{21} and D_{22} can be represented in the following expression.

$$D_{11} = \begin{bmatrix} -D_\alpha S & D_\alpha S D_{p1}M \\ 0 & 0 \end{bmatrix}, \quad D_{12} = \begin{bmatrix} D_\alpha S D_{p2}T \\ I \end{bmatrix}$$

$$D_{21} = [-D_\alpha S \quad D_\alpha S D_{p1}M], \quad D_{22} = D_\alpha S D_{p2}T \quad \dots (40)$$

The sensitivity weight W_s and the complementary sensitivity weight W_t are designed in the same manner as in the first embodiment, and multiplied by the output part of the expression (11), and through γ iteration, the controller K is obtained in the state space representation. The actual controller mounted in the plants such as distillation tower is the controller K multiplied by the weight matrix S , the

weight $\alpha^{-1}I$ and the scaling matrix T , as shown in Fig. 13.

Referring now to Fig. 11, the above operation will be described below. The operation of the control object model input unit 1, the control object model registration unit 2, the frequency response calculation unit 4 and the scaling matrix calculation unit 5 is exactly the same as in the first or second embodiment. A memory unit 3a stores the formulae of the generalized plant of Fig. 12 and the formulae of the control object model that is part of the generalized plant, as described in the expressions (1) to (5), (11), and (32) to (40). The control variable weight W_{yL} for the L -th controlled variable y_L is set in the control variable weight input unit 7 by the user of the design device. This control variable weight W_{yL} is set for each controlled variable y . The control variable weight registration unit 8 outputs the control variable weight W_{yL} input from the control variable weight input unit 7 to the weight matrix calculation unit 9. The weight matrix calculation unit 9 calculates the weight matrix S , based on the control variable weight W_{yL} , employing the expressions (29) and (30), and outputs it to a controller calculation unit 6a. The controller calculation unit 6a registers the scaling matrix T and the weight matrix S in the formulae of the generalized plant stored in the memory unit 3a, and through γ iteration, calculates the parameters of the controller K . At this time, the complementary sensitivity weight W_t , the sensitivity weight W_s and the scaling matrix M are preset in the generalized plant in the

memory unit 3a. In this way, the controller K can be designed.

As described above, in this third embodiment, each controlled variable y can be directly weighted by introducing the weight matrix S. Thereby, the controller with higher control performance and enhanced stability can be designed. Also, there is no need of providing the scaling matrix T with a role of weighting the controlled variable y by introducing the weight matrix S.

Fourth embodiment

In the third embodiment, the control variable weight adjusting means 20 (weight matrix S) is provided inside the closed loop system, but may be provided outside the closed loop system. Fig. 14 is a block diagram showing the configuration of the generalized plant in a fourth embodiment of the present invention. In this fourth embodiment, the control variable weight adjusting means 20 (weight matrix S) is provided at the former stage of the frequency sensitivity weight adjusting means 13. A method for determining the weight matrix S is exactly the same as the method for determining in the third embodiment as described in the expressions (29) and (30).

Next, in this fourth embodiment, the configuration of the generalized plant is modified as shown in Fig. 14, so that the expression (4) can be rewritten into the following expression.

$$z_1' = S e z \quad \dots (41)$$

Thereby, the expression (9) can be rewritten in the

following expression.

$$\begin{bmatrix} z_1' \\ z_2 \end{bmatrix} = \begin{bmatrix} S D_\alpha C_p & S C_\alpha \\ 0 & 0 \end{bmatrix} \begin{bmatrix} x_p \\ x_\alpha \end{bmatrix} + \begin{bmatrix} -S D_\alpha & S D_\alpha D_{p1} M & S D_\alpha D_{p2} T \\ 0 & 0 & I \end{bmatrix} \begin{bmatrix} r \\ w \\ u \end{bmatrix} \quad \dots (42)$$

Representing the expressions (8), (10) and (42) in the
5 Doile's notation as in the expression (11), the parameters
C₁ and C₂ in the expression (11) can be represented in the
following expression.

$$C_1 = \begin{bmatrix} S D_\alpha C_p & S C_\alpha \\ 0 & 0 \end{bmatrix}, \quad C_2 = [D_\alpha C_p \quad C_\alpha] \quad \dots (43)$$

10 Also, the parameters D₁₁, D₁₂, D₂₁ and D₂₂ can be
represented in the following expression.

$$D_{11} = \begin{bmatrix} -S D_\alpha & S D_\alpha D_{p1} M \\ 0 & 0 \end{bmatrix}, \quad D_{12} = \begin{bmatrix} S D_\alpha D_{p2} T \\ I \end{bmatrix}$$

$$D_{21} = [-D_\alpha \quad D_\alpha D_{p1} M], \quad D_{22} = D_\alpha D_{p2} T \quad \dots (44)$$

The parameters A, B₁ and B₂ are the same as shown in the
15 expressions (12) and (13). In this fourth embodiment, the
actual controller mounted in the plants such as distillation
tower is the controller K multiplied by the weight α⁻¹I and
the scaling matrix T, as shown in Fig. 6.

In this fourth embodiment, the configuration of the
20 design device is almost the same as in the third embodiment.
Thus, the operation of the design device of this fourth

embodiment will be described below with reference to Fig.
11.

The operation of the control object model input unit
1, the control object model registration unit 2, the frequency
5 response calculation unit 4 and the scaling matrix
calculation unit 5 is exactly the same as in the first or
second embodiment. A memory unit 3a stores the formulae of
the generalized plant of Fig. 14 and the formulae of the
control object model that is part of the generalized plant,
10 as described in the expressions (1) to (3), (5) to (8), (10)
to (13), and (41) to (44). The operation of the control
variable weight input unit 7, the control variable weight
registration unit 8 and the weight matrix calculation unit
9 is exactly the same as in the third embodiment. The
15 controller calculation unit 6a registers the scaling matrix
T and the weight matrix S in the formulae of the generalized
plant stored in the memory unit 3a, and through γ iteration,
calculates the parameters of the controller K. In this way,
the controller K can be designed.

20 In this fourth embodiment, the control variable weight
adjusting means 20 (weight matrix S) is provided at the former
stage of the frequency sensitivity weight adjusting means
13, but may be provided at the latter stage of the frequency
sensitivity weight adjusting means 13. Since the magnitudes
25 of the gains of the control object model 11 are made consistent
by the scaling matrix T, the weight matrix S can be easily
adjusted, and it is prerequisite that the method for

determining the scaling matrix T as described in the first or second embodiment is employed in the third or fourth embodiment.

Fifth embodiment

5 Fig. 15 is a block diagram showing the configuration of a design device of a controller in a fifth embodiment of the present invention. The design device of Fig. 15 comprises a transient response parameter input unit 101 for inputting the transient response parameters indicating the transient
10 response characteristics of a closed loop system composed of the control objects and the controller, a transient response parameter registration unit 102 for registering the transient response parameters within the device, a closed loop transfer function calculation unit 103 for calculating
15 the transient response characteristics of the closed loop system based on the transient response parameters input from the transient response parameter registration unit 102, a frequency sensitivity weight calculation unit 104 for calculating the frequency sensitivity weight for determining
20 the set value followup characteristic of the closed loop system, based on the transient response characteristics of the closed loop system, and a controller calculation unit 105 for calculating the parameters of the controller by applying the frequency sensitivity weight to the preset
25 generalized plants. The transient response parameter input unit 101, the transient response parameter registration unit 102 and the closed loop transfer function calculation unit

103 constitute setting means for setting the transient response characteristics of the closed loop system.

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An algorithm for designing the controller in accordance with the H_∞ logic is designed based on the generalized plants as represented using the control objects. Therefore, the generalized plants will be first described. Fig. 16 is a block diagram showing the configuration of a model of an actual control object as represented in the formulae. A numerical model of the control object as shown in Fig. 16 is composed of a model 111 for the manipulated variable u and a model 112 for the disturbance w . Reference sign P_u denotes a transfer function of the model 111 and reference sign P_w denotes a transfer function of the model 112. The models 111, 112 are obtained as a result of the model identification using the data obtained by a step response test for the actual control object. The controlled variable y that is the output of control object is a sum of the outputs from the models 111 and 112.

Fig. 17 shows the configuration of the conventional generalized plants containing such numerical model of control object. The generalized plants involve providing a frequency weight called a sensitivity weight W_s used to determine the set value followup characteristic and a frequency weight called a complementary sensitivity weight W_t used to determine the robust stability, and introducing the set value r , and the outputs z_1 , z_2 in addition to the input (manipulated variable) u of control object, input

(disturbance) w , and output (controlled variable) y , to realize both the set value followup characteristic and the robust stability as shown in Fig. 17. Deviation e ($=y-r$) is an observation quantity or the input into the controller (not shown). Reference numeral 113 denotes a block representing the sensitivity weight W_s , and reference sign Z_1 denotes an output for effecting the evaluation of the set value followup characteristic. Also, reference numeral 114 denotes a block representing the complementary sensitivity weight W_t , and reference sign Z_2 denotes an output for effecting the evaluation of the robust stability.

Conventionally, in the generalized plants as shown in Fig. 17, the complementary sensitivity weight W_t is determined by estimating the uncertainty of the models on the basis of the numerical models of control objects, the sensitivity weight W_s is determined by directly specifying the frequency characteristic in view of the followupability to the set value r , whereby the parameters of the controller are determined through the γ iteration. However, since employing the generalized plants of Fig. 17, the controller is designed on the basis of a larger gain due to differences in the gains for the plant outputs of the manipulated variables, the obtained controller is likely to be very conservative, or excessively stable. Also, since the set value followup characteristic and the disturbance response characteristic are usually reciprocal, it is preferred to design with the weight according to the purpose rather than

with the same weight. Further, in the generalized plants of Fig. 17 containing no integral element, some steady-state deviation arises. If the sensitivity weight W_s is provided with the integral characteristic, the controller can have the integral characteristic, but the generalized plants become unstable, not leading to the normal H_∞ problem.

Therefore, in this fifth embodiment, the generalized plant as shown in Fig. 18 is considered. In Fig. 18, reference sign M denotes a scaling matrix for adjusting the influence of disturbance w on the controlled variable y , reference sign T denotes a scaling matrix for making the magnitudes of errors of the control objects consistent, and reference sign $\alpha^{-1}I$ denotes a weight for providing the controller with the integral characteristic to eliminate the steady-state deviation. Herein, $\alpha(s)$ is defined as $\alpha(s) = s/(s+a)$. Where s is a Laplace operator, and a (>0) is any real number. Reference numeral 115 denotes a block representing the scaling matrix M, reference numeral 116 denotes a block representing the scaling matrix T, and reference numeral 117 denotes a block representing the weight $\alpha^{-1}I$. Deviation e_2 is deviation e multiplied by the weight $\alpha^{-1}I$, and input into the controller. Fig. 19 shows the configuration of a robust control system in which a controller K is added to the above generalized plant. In Fig. 19, reference numeral 118 denotes a block representing the controller K.

The design device of the controller in this fifth embodiment is aimed at determining the parameters of the

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controller K such that the controlled variable y that is the output of control object follows the set value r, the influence of disturbance w is removed, and the control object is stabilized even if it is fluctuated or there is an error in the model of control object. The H_∞ control problem can be regarded as the problem of reducing the H_∞ norm (gain) of the transfer function from (r, w) to (z_1 , z_2). That is, the set value followup characteristic, the robust stability and the disturbance suppression may be considered in the following way.

(D) Set value followup characteristic: If the H_∞ norm (gain) of the transfer function from the set value r to deviation e (more correctly, transfer function with the set value r multiplied by the frequency weight $\alpha^{-1}W_s$ from r to z_1) is reduced, the deviation e can be decreased, so that the set value followup characteristic can be made better. Herein, $\alpha^{-1}W_s$ is the frequency weight for restricting the followup band (e.g., followup only in the low band).

(E) Robust stability: There is an error between the actual control object and its model due to characteristic variations of the control object or the error at the time of modeling. The maximum value of the error from the identified model is estimated as $\Delta(s)$, and the controller K is designed such that the H_∞ norm from the set value r to z_2 is smaller than or equal to 1, employing the complementary sensitivity weight $W_t(s)$ such that $|\Delta(j\omega)| < |W_t(j\omega)|$ for this error, whereby the robust

stabilization can be achieved.

(F) Disturbance suppression: If the H_∞ norm (gain) of the transfer function from disturbance w to deviation e (more correctly, transfer function with the disturbance w multiplied by the frequency weight $\alpha^{-1}W_s$ from w to z_1) is reduced, the deviation e can be decreased even if the disturbance w enters, whereby the disturbance suppression can be ameliorated.

Next, it is supposed that the state space representation of the generalized plant as shown in Fig. 18 is given by:

$$\dot{x}_p = A_p x_p + B_{p1} M w + B_{p2} T u \quad \dots (101)$$

$$y = C_p x_p + D_{p1} M w + D_{p2} T u \quad \dots (102)$$

In the above expressions (101) and (102), x_p is the quantity of state, and A_p , B_{p1} , B_{p2} , C_p , D_{p1} and D_{p2} are the parameters of the numerical models 111, 112 of control objects. From the expression (102), the deviation e can be obtained in the following expression.

$$e = y - r = C_p x_p + D_{p1} M w + D_{p2} T u - r \quad \dots (103)$$

With the configuration of the generalized plant as shown in Fig. 18, the outputs z_1' and z_2' can be defined in the following expressions.

$$z_1' = e \quad \dots (104)$$

$$z_2' = u \quad \dots (105)$$

The frequency weight for providing the controller K with the integral characteristic can be defined in the following

expression, using the expression (103).

$$\begin{aligned} \dot{x}_\alpha &= A_\alpha x_\alpha + B_\alpha e \\ &= A_\alpha x_\alpha + B_\alpha C_p x_p + B_\alpha D_{p1} M w + B_\alpha D_{p2} T u - B_\alpha r \quad \dots (106) \end{aligned}$$

$$\begin{aligned} e_2 &= C_\alpha x_\alpha + D_\alpha e \\ &= C_\alpha x_\alpha + D_\alpha C_p x_p + D_\alpha D_{p1} M w + D_\alpha D_{p2} T u - D_\alpha r \quad \dots (107) \end{aligned}$$

In the expressions (106) and (107), x_α is the quantity of state of $\alpha^{-1}I$, and A_α , B_α , C_α and D_α are the parameters of $\alpha^{-1}I$. Arranging the above expressions and representing them in a state space, the following three expressions can be obtained.

$$\frac{d}{dt} \begin{bmatrix} x_p \\ x_\alpha \end{bmatrix} = \begin{bmatrix} A_p & 0 \\ B_\alpha C_p & A_\alpha \end{bmatrix} \begin{bmatrix} x_p \\ x_\alpha \end{bmatrix} + \begin{bmatrix} 0 & B_{p1} M & B_{p2} T \\ -B_\alpha & B_\alpha D_{p1} M & B_\alpha D_{p2} T \end{bmatrix} \begin{bmatrix} r \\ w \\ u \end{bmatrix} \quad \dots (108)$$

$$\begin{bmatrix} z_1' \\ z_2' \end{bmatrix} = \begin{bmatrix} D_\alpha C_p & C_\alpha \\ 0 & 0 \end{bmatrix} \begin{bmatrix} x_p \\ x_\alpha \end{bmatrix} + \begin{bmatrix} -D_\alpha & D_\alpha D_{p1} M & D_\alpha D_{p2} T \\ 0 & 0 & I \end{bmatrix} \begin{bmatrix} r \\ w \\ u \end{bmatrix} \quad \dots (109)$$

$$e_2 = \begin{bmatrix} D_\alpha C_p & C_\alpha \end{bmatrix} \begin{bmatrix} x_p \\ x_\alpha \end{bmatrix} + \begin{bmatrix} -D_\alpha & D_\alpha D_{p1} M & D_\alpha D_{p2} T \end{bmatrix} \begin{bmatrix} r \\ w \\ u \end{bmatrix} \quad \dots (110)$$

10

Representing the expressions (108), (109) and (110) in Doile's notation, the following expression can be obtained.

$$G(s) = \begin{bmatrix} A & B_1 & B_2 \\ C_1 & D_{11} & D_{12} \\ C_2 & D_{21} & D_{22} \end{bmatrix} \quad \dots (111)$$

Parameter A can be represented as follows:

$$A = \begin{bmatrix} A_p & 0 \\ B_\alpha C_p & A_\alpha \end{bmatrix} \quad \dots (112)$$

Parameters B_1 and B_2 can be represented as follows:

5

$$B_1 = \begin{bmatrix} 0 & B_{p1}M \\ -B_\alpha & B_\alpha D_{p1}M \end{bmatrix}, \quad B_2 = \begin{bmatrix} B_{p2}T \\ B_\alpha D_{p2}T \end{bmatrix} \quad \dots (113)$$

Also, parameters C_1 and C_2 can be represented as follows:

$$C_1 = \begin{bmatrix} D_\alpha C_p & C_\alpha \\ 0 & 0 \end{bmatrix}, \quad C_2 = [D_\alpha C_p \quad C_\alpha] \quad \dots (114)$$

10

And the parameters D_{11} , D_{12} , D_{21} , D_{22} can be represented as follows:

$$D_{11} = \begin{bmatrix} -D_\alpha & D_\alpha D_{p1}M \\ 0 & 0 \end{bmatrix}, \quad D_{12} = \begin{bmatrix} D_\alpha D_{p2}T \\ I \end{bmatrix}$$

$$D_{21} = [-D_\alpha \quad D_\alpha D_{p1}M], \quad D_{22} = D_\alpha D_{p2}T \quad \dots (115)$$

The sensitivity weight W_s and the complementary
 15 sensitivity weight W_t are designed, and multiplied by the
 output parts of the expression (111). Through γ iteration,
 the controller K is obtained in the state space representation.
 Herein, the output parts of the expression (111) signify the
 parts corresponding to the outputs z_1' , z_2' in Fig. 18. Hence,
 20 an output equation of the parameters C_1 , D_{11} , D_{12} of the
 expression (111) may be multiplied by a diagonal matrix Q
 as represented in the following expression having the

diagonal elements of sensitivity weight W_s and complementary sensitivity weight W_t from the left side. Thus, the parameters of the controller K can be calculated.

$$Q = \begin{bmatrix} W_s & 0 \\ 0 & W_t \end{bmatrix} \quad \dots (116)$$

5

The controller K is a solution of the H_∞ control problem with the generalized plants, and the actual controller mounted on the plants such as a distillation tower is the controller K multiplied by weight $\alpha^{-1}I$ and scaling matrix T , as shown in Fig. 20.

10

As previously described, the H_∞ logic is a design method in the frequency domain. Therefore, the design is easy in the control of the mechanical system, but is hard in the control system untreatable in the frequency domain such as the process control, and it is difficult to suitably select the complementary sensitivity weight W_t and the sensitivity weight W_s . In the following, a method for determining the complementary sensitivity weight W_t in this embodiment will be described below. The control object is varied in the characteristics, depending on the driving conditions.

Normally, the control design is made based on a certain model, but in the robust control design, the variation of control object and the magnitude of error of modeling are contained beforehand in the control design, and the controller is designed to be stable without much deterioration in the control performance even if there is any variation or error.

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Fig. 21 shows an additive error for the model 111 of control object. In Fig. 21, reference numeral 119 denotes a block representing the additive error Δ . In the robust control design, a variation in the characteristic of the control object owing to the driving conditions and a model error due to lower dimension of the model 111 are represented as the additive error Δ as shown in Fig. 21. If the characteristics of the control object are deviated from the model 111 due to this additive error Δ , the controller is designed such that the controller output may be stable. To this end, the complementary sensitivity weight W_t may be determined to cover the additive error Δ . The general expression of this complementary sensitivity weight W_t is shown in the following expression. Since the change of the model 112 is not related with the stability of the system, it is supposed that the model 111 alone is varied in designing the controller.

$$W_t = \begin{bmatrix} W_{t1} & 0 & 0 & \dots & 0 \\ 0 & W_{t2} & 0 & \dots & 0 \\ 0 & 0 & W_{t3} & \dots & 0 \\ \vdots & \vdots & \vdots & \ddots & \vdots \\ 0 & 0 & 0 & \dots & W_{tN} \end{bmatrix} \quad \dots (117)$$

In this fifth embodiment, for the additive error Δ with scaled magnitude, employing the scaling matrix T , the element of the complementary sensitivity weight W_t is the maximum value G_{\max} of the gains of error Δ multiplied by a safety factor δ (δ is equal to 1, for example). Namely, the elements (weights) W_{t1} , W_{t2} , W_{t3} , ..., W_{tN} are defined as follows:

$$W_{1,1}=W_{1,2}=W_{1,3}=W_{1,N}=(1+\delta) \text{ G m a x} \quad \cdot \cdot \cdot (118)$$

This embodiment is involved with the multivariable control system, and assuming that the number of manipulated variables u is N (N is a positive integer), the complementary sensitivity weight W_t is $N \times N$ matrix. Where W_{tN} is the weight for the N -th manipulated variable u_N .

Next, the methods for determining the scaling matrices T , M will be described below. A general expression of the scaling matrix T is shown in the following expression.

$$T = \begin{bmatrix} T_1 & 0 & 0 & \dots & 0 \\ 0 & T_2 & 0 & \dots & 0 \\ 0 & 0 & T_3 & \dots & 0 \\ \vdots & \vdots & \vdots & \ddots & \vdots \\ 0 & 0 & 0 & \dots & T_N \end{bmatrix} \quad \cdot \cdot \cdot (119)$$

Assuming that the number of manipulated variables u is N , the scaling matrix T is $N \times N$ matrix. Element T_N of the scaling matrix T is the weight for the N -th manipulated variable u_N . Each element T_N is determined such that the magnitudes of the components of the additive error Δ are as equal as possible.

Next, a general expression of the scaling matrix M is shown in the following expression.

$$M = \begin{bmatrix} M_1 & 0 & 0 & \dots & 0 \\ 0 & M_2 & 0 & \dots & 0 \\ 0 & 0 & M_3 & \dots & 0 \\ \vdots & \vdots & \vdots & \ddots & \vdots \\ 0 & 0 & 0 & \dots & M_J \end{bmatrix} \quad \cdot \cdot \cdot (120)$$

Assuming that the number of disturbance w is J (J is

a positive integer), the scaling matrix M is $J \times J$ matrix. Element M_J of the scaling matrix M is the weight for the J -th disturbance w_J . Each element M_J is an adjustment parameter for determining the disturbance suppression performance by
 5 adjusting the influence of each disturbance w_J on the controlled variable y .

Next, a method for determining the sensitivity weight W_s in this fifth embodiment will be described below. First of all, a general expression of the sensitivity weight W_s is
 10 shown in the following expression.

$$W_s = \begin{bmatrix} W_{s1} & 0 & 0 & \dots & 0 \\ 0 & W_{s2} & 0 & \dots & 0 \\ 0 & 0 & W_{s3} & \dots & 0 \\ \vdots & \vdots & \vdots & \ddots & \vdots \\ 0 & 0 & 0 & \dots & W_{sL} \end{bmatrix} \quad \dots (121)$$

Assuming that the number of controlled variables y is L (L is a positive integer), the sensitivity weight W_s is $L \times L$ matrix. Element W_{sL} of the sensitivity weight W_s is the weight
 15 for the L -th controlled variable y_L . In order to determine the sensitivity weight W_s , a closed loop system of Fig. 22 in which the robust control system of Fig. 19 is simplified is considered. In Fig. 22, reference numeral 111a denotes
 20 a block representing a numerical model P of control object, and reference numeral 113a denotes a block representing the frequency weight W_s' .

Supposing that the sensitivity function indicating the control performance mainly regarding the quick-response

property such as the set value followupability or disturbance suppression is $S(s)$, the smaller gain $|S(j\omega)|$ of the sensitivity function $S(s)$ is preferable because the model variations have less effect on the set value response. If the control specification at each frequency is given by $S_{\text{spec}}(\omega)$, the following condition concerning the sensitivity function $S(s)$ can be obtained.

$$|S(j\omega)| < S_{\text{spec}}(\omega); \quad \forall \omega \quad \dots (122)$$

Where $\forall \omega$ means that the expression (122) holds for all frequencies ω .

On one hand, the sensitivity function $S(s)$ corresponds to the transfer function $G_{\text{er}}(s)$ of the closed loop system from the set value r to deviation e , as shown in Fig. 22. Supposing that the transfer function of control object is $P(s)$ and the transfer function of controller is $K(s)$, the following expression is obtained.

$$S(s) = G_{\text{er}}(s) = \frac{-1}{1 - P(s)K(s)} \quad \dots (123)$$

Also, the transfer function $G_{\text{yr}}(s)$ of the closed loop system of Fig. 22 from the set value r to the controlled variable y is obtained in the following expression.

$$G_{\text{yr}}(s) = \frac{-P(s)K(s)}{1 - P(s)K(s)} \quad \dots (124)$$

From the expressions (123) and (124), the sensitivity function $S(s)$ can be obtained in the following expression.

$$S(s) = G_{yr}(s) - 1 \quad \dots (125)$$

In this fifth embodiment, the transient response characteristic of the closed loop system as shown in Fig. 22, or the transfer function $G_{yr}(s)$ of the closed loop system from the set value r to the controlled variable y is approximated with a first-order lag characteristic as in the following expression, giving $G_{yr-spec}(s)$ as the specification of the transfer function $G_{yr}(s)$.

$$G_{yr-spec}(s) = \frac{1}{T_{sL}s + 1} \quad \dots (126)$$

In the expression (126), T_{sL} is a time constant regarding the L -th controlled variable y_L . Employing $G_{yr-spec}(s)$ in the expression (126), instead of $G_{yr}(s)$ in the expression (125), the following control specification $S_{spec}(s)$ is obtained.

$$S_{spec}(s) = -\frac{T_{sL}s}{T_{sL}s + 1} \quad \dots (127)$$

In this fifth embodiment, the frequency weight $W_{sL}'(s)$ regarding the L -th controlled variable y_L is set as follows:

$$W_{sL}'(s) = \frac{1}{S_{spec}(s)} = -\frac{T_{sL}s + 1}{T_{sL}s} \quad \dots (128)$$

The frequency weight $W_{sL}'(s)$ is $W_{sL}(s)$ multiplied by $\alpha^{-1}(s)$, and defined as follows:

$$W_{sL}'(s) = \alpha^{-1}(s)W_{sL}(s) \quad \dots (129)$$

If the frequency weight $W_{sL}'(s)$ is set as in the expression (128), the expression (122) can be transformed into the following expression.

$$|S(j\omega)| < \frac{1}{|W_{sL}'(j\omega)|}; \forall \omega \quad \dots (130)$$

Further, the expression (130) can be rewritten into the following expression, using the H_∞ norm.

$$\|W_{sL}'(s)S(s)\|_\infty < 1 \quad \dots (131)$$

The expression (131) indicates that the H_∞ norm of the transfer function of the closed loop system of Fig. 22 from the set value r to the deviation e (more correctly, the transfer function with the set value r multiplied by the frequency weight $\alpha^{-1}(s)W_{sL}(s)$ from r to z_1) is less than 1. This expression (131) is a design index of the controller

K in view of the set value followup characteristic.

Accordingly, by setting the frequency weight $W_{sL}'(s)$ in accordance with the expression (128), the expression (131) is satisfied, whereby the controller K can be designed in view of the set value followup characteristic. If the expression (128) is transformed, the following expression is obtained.

$$W_{sL}'(s) = \frac{s+a}{s} \cdot \frac{-(T_{sL}s+1)}{T_{sL}(s+a)} \quad \dots (132)$$

The first term on the right side of the expression (132)

is $\alpha^{-1}(s)$. Therefore, element $W_{sL}(s)$ of the sensitivity weight W_s can be calculated as follows:

$$W_{sL}(s) = -\frac{T_{sL}s + 1}{T_{sL}(s + a)} \quad \dots (133)$$

- 5 Substituting the expression (133), the expression (121) can be represented as follows:

$$W_s = \begin{bmatrix} -\frac{T_{s1}s + 1}{T_{s1}(s + a)} & 0 & 0 & \dots & 0 \\ 0 & -\frac{T_{s2}s + 1}{T_{s2}(s + a)} & 0 & \dots & 0 \\ 0 & 0 & -\frac{T_{s3}s + 1}{T_{s3}(s + a)} & \dots & 0 \\ \vdots & \vdots & \vdots & \ddots & \vdots \\ 0 & 0 & 0 & \dots & -\frac{T_{sL}s + 1}{T_{sL}(s + a)} \end{bmatrix} \quad \dots (134)$$

In this way, the sensitivity weight W_s can be determined.

- 10 Referring now to Fig. 15, the above operation will be described below. The transient response parameter or the time constant T_{sL} is set in the transient response parameter input unit 101 by the user of the design device. The time constant T_{sL} is set for each controlled variable y . The transient response parameter registration unit 102 outputs the time constant T_{sL} input from the transient response parameter input unit 101 directly to the closed loop transfer function calculation unit 103. The closed loop transfer function calculation unit 103 calculates the transfer function $G_{yr}(s)$ of the closed loop system as shown in Fig. 22 from the set
- 15
- 20

value r to the controlled variable y by substituting the input time constant T_{sL} into the expression (126), and outputs it to the frequency sensitivity weight calculation unit 104. Subsequently, the frequency sensitivity weight calculation unit 104 calculates the sensitivity weight W_s , based on the transfer function $G_{yr}(s)$, employing the expressions (125), (127), (128), and (132) to (134), and outputs it to the controller calculation unit 105. The memory unit 106 stores the formulae of generalized plants as described in the expressions (101) to (115) and shown in Fig. 18. The controller calculation unit 105 registers the sensitivity weight W_s in the formulae of the generalized plants stored in the memory unit 106, and through γ iteration, calculates the parameters of the controller K . At this time, the complementary sensitivity weight W_t , and the scaling matrices T , M are preset in the generalized plants in the memory unit 106. In this way, the controller K can be designed.

As previously described, in the process control field, it is difficult to give the control specification in the frequency domain, and to determine the frequency sensitivity weight W_s . On the contrary, in this embodiment, the transient response characteristic (transfer function $G_{yr}(s)$) of the closed loop system is set, and the frequency weight W_s can be calculated, based on this transient response characteristic. Thereby, even in the process control field, where the frequency response characteristic is difficult to give as the control specification, the controller can be

designed in accordance with the H_∞ logic. Consequently, the multivariable control system can be easily designed in view of the variations of the control objects and the uncertainty of the numerical models. Also, the controller can be realized
5 utilizing the features of the H_∞ logic with smaller computational load during execution of the control, and with which the small-scale control system can be implemented. By approximating the transient response characteristic of the closed loop system with a first-order lag characteristic,
10 the parameters for the control design are intuitively understandable to the designer. Therefore, the design device that is easily understood and used by the designer can be realized. Since the parameters are intuitively understandable to the designer, the design device that is
15 capable of changing the design can be realized in the case where the controller is redesigned after designed once.

Sixth embodiment

In the fifth embodiment, the transient response characteristic of the closed loop system is approximated with
20 a first-order lag, and the sensitivity weight W_s is determined by specifying the time constant of the closed loop system for the controlled variables. In this case, albeit the control design based on the transient response characteristic, only one design parameter is specified for each controlled
25 variable, and the obtained control system does not necessarily operate with the first-order lag as specified. Considering the practicality of the multivariable control,

it is not favorable to increase the number of design parameters, but if the degree of freedom for the design is increased by making the meanings of design parameters clear, it may not be necessarily a false policy. Thus, in this sixth embodiment, the controller is designed by approximating the characteristics of the closed loop system with a second-order system as commonly used, and specifying the transient response characteristic parameters.

Firstly, the transient response of the closed loop system of Fig. 22 for each controlled variable is approximated with the second-order system in the following expression.

$$\frac{y}{r} = \frac{\omega_n^2}{s^2 + 2\zeta\omega_n s + \omega_n^2} \quad \dots (135)$$

In the expression (135), ζ ($\zeta > 0$) is a damping coefficient, and ω_n ($\omega_n > 0$) is a natural frequency. The solution of the characteristic equation of the system as indicated in the expression (135) is obtained in the following expression.

$$s = -\zeta\omega_n \pm \omega_n\sqrt{\zeta^2 - 1} \quad \dots (136)$$

Giving a step input ($r(s) = 1/s$), the controlled variable $y(s)$ that is an output of the closed loop system can be obtained in the following expression.

$$\begin{aligned} y(s) &= \frac{\omega_n^2}{(s - s_1)(s - s_2)} \cdot \frac{1}{s} \\ &= \frac{1}{s} + \frac{C_1}{s + \zeta\omega_n - \omega_n\sqrt{\zeta^2 - 1}} + \frac{C_2}{s + \zeta\omega_n + \omega_n\sqrt{\zeta^2 - 1}} \quad \dots (137) \end{aligned}$$

The parameters s_1, s_2, C_1, C_2 in the expression (137) are given in the following expression.

$$s_1 = -\zeta \omega_n + \omega_n \sqrt{\zeta^2 - 1} \quad , \quad s_2 = -\zeta \omega_n - \omega_n \sqrt{\zeta^2 - 1}$$

$$C_1 = \frac{-\zeta - \sqrt{\zeta^2 - 1}}{2\sqrt{\zeta^2 - 1}} \quad , \quad C_2 = \frac{\zeta - \sqrt{\zeta^2 - 1}}{2\sqrt{\zeta^2 - 1}} \quad \dots (138)$$

Consider the most important damped oscillation ($0 < \zeta < 1$) in the second-order system characteristic. Then, the parameters C_1, C_2 are given in the following expression.

$$C_1 = \frac{i(\zeta + i\sqrt{1 - \zeta^2})}{2\sqrt{1 - \zeta^2}} \quad , \quad C_2 = \frac{i(-\zeta + i\sqrt{1 - \zeta^2})}{2\sqrt{1 - \zeta^2}} \quad \dots (139)$$

Thereby, the time response of the closed loop system as shown in Fig. 22 can be represented in the following expression.

$$\begin{aligned}
 y(t) &= 1 + \frac{i(\zeta + i\sqrt{1-\zeta^2})}{2\sqrt{1-\zeta^2}} \cdot \exp(-\zeta \omega_n + i \omega_n \sqrt{1-\zeta^2})t \\
 &\quad + \frac{i(-\zeta + i\sqrt{1-\zeta^2})}{2\sqrt{1-\zeta^2}} \cdot \exp(-\zeta \omega_n - i \omega_n \sqrt{1-\zeta^2})t \\
 &= 1 + \frac{i(\zeta + i\sqrt{1-\zeta^2})}{2\sqrt{1-\zeta^2}} \cdot e^{-\zeta \omega_n t} \left(\cos \omega_n \sqrt{1-\zeta^2} t + i \sin \omega_n \sqrt{1-\zeta^2} t \right) \\
 &\quad + \frac{i(-\zeta + i\sqrt{1-\zeta^2})}{2\sqrt{1-\zeta^2}} \cdot e^{-\zeta \omega_n t} \left(\cos \omega_n \sqrt{1-\zeta^2} t - i \sin \omega_n \sqrt{1-\zeta^2} t \right) \\
 &= 1 - e^{-\zeta \omega_n t} \left(\cos \omega_n \sqrt{1-\zeta^2} t + \frac{\zeta}{\sqrt{1-\zeta^2}} \sin \omega_n \sqrt{1-\zeta^2} t \right) \\
 &= 1 - \frac{e^{-\zeta \omega_n t}}{\sqrt{1-\zeta^2}} \sin \left(\omega_n \sqrt{1-\zeta^2} t + \psi \right), \quad \psi = \cos^{-1} \zeta \quad \dots (140)
 \end{aligned}$$

One embodiment of the time response of the closed loop system as represented in the expression (140) is shown in Fig. 23. Fig. 23 shows how the controlled variable y behaves when a 100% step set value r is given at time 0. The parameters representing the typical transient response characteristic of the second-order system corresponding to this time response include a rise time t_r for which the controlled variable y reaches the same value as the set value r (herein 100%), the overshoot OS that is an extreme value of the transient deviation firstly taken after the controlled variable y exceeds the set value r , the overshoot time t_p for which the controlled variable y reaches the overshoot OS, the settling time t_q for which the controlled variable y is contained within 5% of a range of the set value r , and the damping ratio DR that is the ratio of a_1 to a_2 as shown in

Fig. 23. The rise time t_r can be represented in the following expression, employing the damping coefficient ζ and the natural frequency ω_n .

$$t_r = \frac{1}{\omega_n \sqrt{1 - \zeta^2}} (\pi - \cos^{-1} \zeta) \quad \dots (141)$$

5 Similarly, the overshoot time t_p is indicated below.

$$t_p = \frac{\pi}{\omega_n \sqrt{1 - \zeta^2}} \quad \dots (142)$$

The settling time t_q can be obtained in the following expression.

$$t_q = \frac{3}{\zeta \omega_n} \quad \dots (143)$$

10 Also, the overshoot OS can be obtained in the following expression, employing the damping coefficient ζ .

$$OS = \exp \left(\frac{-\zeta \pi}{\sqrt{1 - \zeta^2}} \right) \quad \dots (144)$$

And the damping ratio DR can be obtained in the following expression.

$$15 \quad DR = a_2 / a_1 = \exp \left(-2 \pi \zeta / \sqrt{1 - \zeta^2} \right) \quad \dots (145)$$

From the expression (135), the transfer function $G_{yr}(s)$ of the closed loop system of Fig. 22 from the set value r to the controlled variable y can be obtained in the following expression.

$$20 \quad G_{yr}(s) = \frac{\omega_n^2}{s^2 + 2 \zeta \omega_n s + \omega_n^2} \quad \dots (146)$$

If the frequency weight $W_{sL}'(s)$ is set in the following expression, as in the fifth embodiment, the expression (131) is satisfied, and the controller K can be designed in view of the set value followup characteristic.

$$W_{sL}'(s) = \frac{1}{S_{spec}(s)} = \frac{1}{G_{yr}(s) - 1} = \frac{1}{\frac{\omega_{nL}^2}{s^2 + 2 \zeta_L \omega_{nL} s + \omega_{nL}^2} - 1} \dots (147)$$

In the expression (147), ζ_L is the damping coefficient for the L -th controlled variable y_L , and ω_{nL} is the natural frequency for the controlled variable y_L . The expression (147) can be transformed into the following expression.

$$\begin{aligned} W_{sL}'(s) &= \frac{s^2 + 2 \zeta_L \omega_{nL} s + \omega_{nL}^2}{-s^2 - 2 \zeta_L \omega_{nL} s} \\ &= \frac{s + a}{s} \cdot \frac{-(s^2 + 2 \zeta_L \omega_{nL} s + \omega_{nL}^2)}{(s + 2 \zeta_L \omega_{nL})(s + a)} \dots (148) \end{aligned}$$

The first term on the right side of the expression (148) is $\alpha^{-1}(s)$. Accordingly, the element $W_{sL}(s)$ of the sensitivity weight W_s can be calculated in the following expression.

$$W_{sL}(s) = -\frac{s^2 + 2 \zeta_L \omega_{nL} s + \omega_{nL}^2}{(s + 2 \zeta_L \omega_{nL})(s + a)} \dots (149)$$

Substituting the expression (149), the expression (121) can be represented as follows:

$$W_s = \begin{bmatrix} -\frac{s^2 + 2\zeta_1\omega_{n1}s + \omega_{n1}^2}{(s + 2\zeta_1\omega_{n1})(s + a)} & 0 & \dots & 0 \\ 0 & -\frac{s^2 + 2\zeta_2\omega_{n2}s + \omega_{n2}^2}{(s + 2\zeta_2\omega_{n2})(s + a)} & \dots & 0 \\ \vdots & \vdots & \ddots & \vdots \\ 0 & 0 & \dots & -\frac{s^2 + 2\zeta_L\omega_{nL}s + \omega_{nL}^2}{(s + 2\zeta_L\omega_{nL})(s + a)} \end{bmatrix} \quad \dots (150)$$

To calculate the sensitivity weight W_s employing the expression (150), it is required to obtain the damping coefficient ζ_L and the natural frequency ω_{nL} . To obtain the damping coefficient ζ_L and the natural frequency ω_{nL} , two items are selected from among the rise time t_r , the overshoot time t_p , the settling time t_q , the overshoot OS and the damping ratio DR, and the two selected parameter values are set. In this sixth embodiment, the method for calculating the damping coefficient ζ_L and the natural frequency ω_{nL} , as one embodiment, will be described with an instance of employing the rise time t_r and the overshoot OS. With the overshoot OS as indicated in the expression (144), the damping coefficient ζ_L can be obtained in the following expression.

$$\zeta_L = \sqrt{\frac{(\ln(OS_L))^2}{\pi^2 + (\ln(OS_L))^2}} \quad \dots (151)$$

In the expression (151), OS_L is the overshoot for the L-th controlled variable y_L . Also, from the rise time t_r as indicated in the expression (141), the natural frequency ω_{nL} can be obtained in the following expression.

$$\omega_{nL} = \frac{\pi - \cos^{-1} \zeta_L}{t_{rL} \sqrt{1 - \zeta_L^2}} \quad \dots (152)$$

In the expression (152), t_{rL} is the rise time for the L-th controlled variable y_L . In this way, if the value of overshoot OS_L is set, the damping coefficient ζ_L can be calculated from the expression (151), and if the value of the rise time t_{rL} is set, the natural frequency ω_{nL} can be calculated from the expression (152). In the above way, the sensitivity weight W_s can be determined.

In this sixth embodiment, the configuration of the design device is most the same as in the fifth embodiment. Thus, the operation of the design device of this sixth embodiment will be described below with reference to Fig. 15. The transient response parameters, i.e., the overshoot OS_L and the rise time t_{rL} , are set into the transient response parameter input unit 101 by the user of the design device. This overshoot OS_L and the rise time t_{rL} are set for each controlled variable y . The transient response parameter registration unit 102 outputs the overshoot OS_L and the rise time t_{rL} input from transient response parameter input unit 101 directly to the closed loop transfer function calculation unit 103. The closed loop transfer function calculation unit 103 calculates the damping coefficient ζ_L and the natural frequency ω_{nL} , based on the overshoot OS_L and the rise time t_{rL} , employing the expressions (151) and (152). Substituting the damping coefficient ζ_L and the natural frequency ω_{nL} into the expression (146), the transfer function $G_{yr}(s)$ is

calculated, and output to the frequency sensitivity weight calculation unit 104. Then, the frequency sensitivity weight calculation unit 104 calculates the sensitivity weight W_s , based on the transfer function $G_{yr}(s)$, employing the expressions (147) to (150), and outputs it to the controller calculation unit 105. The operation of the controller calculation unit 105 and the memory unit 106 is exactly the same as in the fifth embodiment. In this way, the controller K can be designed.

10 As described above, in this sixth embodiment, the degree of freedom in the design can be increased by approximating the transient response characteristic of the closed loop system with the second-order system characteristic, and the controller provided by the design device can have wider applicability. The first to sixth embodiments are involved with the design device which designs the multivariable controller. Also, the design device of the first to sixth embodiments can be implemented on the computer. That is, the computer is equipped with an operation unit, a storage device and an input/output device, and operates as the design device in accordance with the program.

Industrial Applicability

As described above, the present invention is suitable for designing the multivariable controller.

CLAIMS

1. A design device for designing a controller in accordance with the H infinity ($H\infty$) control logic, employing the generalized plants having the control object models for the manipulated variables, characterized by comprising:

storage means for storing said generalized plants;
parameter calculating means for calculating the parameters of components of said generalized plants in accordance with the response characteristic of said control object model or the response characteristic of a closed loop system consisting of said control object model and said controller; and

controller calculation means for calculating said controller by applying said parameters to said generalized plants stored in said storage means.

2. The design device of controller according to claim 1, characterized in that said generalized plants have said control object model, and manipulated variable weight adjusting means for adjusting the input of manipulated variable into said control object model, which is provided in the former stage of said control object model, said parameter calculating means comprises frequency response calculation means for calculating the frequency responses of said control object models, and scaling matrix calculation means for calculating a scaling matrix T for determining the weighting of said manipulated variables with said manipulated variable weight adjusting means in accordance

with the frequency responses of said control object models
so that the respective gains of said control object models
are consistent, and said controller calculation means
calculates the controller by applying said scaling matrix
5 T to the manipulated variable weight adjusting means of said
generalized plants stored in said storage means.

3. The design device of controller according to claim
2, characterized in that said scaling matrix calculation
means calculates said scaling matrix T as follows:

$$T = \begin{bmatrix} T_1 & 0 & 0 & \dots & 0 \\ 0 & T_2 & 0 & \dots & 0 \\ 0 & 0 & T_3 & \dots & 0 \\ \vdots & \vdots & \vdots & \ddots & \vdots \\ 0 & 0 & 0 & \dots & T_N \end{bmatrix}$$

$$T_N = \frac{1}{L} \cdot \frac{\max(\|G_{y1u1}\|_\infty, \|G_{y1u2}\|_\infty, \dots, \|G_{y1uN}\|_\infty)}{\|G_{y1uN}\|_\infty}$$

$$+ \frac{1}{L} \cdot \frac{\max(\|G_{y2u1}\|_\infty, \|G_{y2u2}\|_\infty, \dots, \|G_{y2uN}\|_\infty)}{\|G_{y2uN}\|_\infty}$$

$$+ \dots + \frac{1}{L} \cdot \frac{\max(\|G_{yLu1}\|_\infty, \|G_{yLu2}\|_\infty, \dots, \|G_{yLuN}\|_\infty)}{\|G_{yLuN}\|_\infty}$$

10

where the number of manipulated variables u is N (N is a
positive integer), the number of controlled variables y is
L (L is a positive integer), and the H_∞ norm of the transfer
function of said control object model from the N-th
15 manipulated variable u_N to the L-th controlled variable y_L
is $\|G_{yLuN}\|_\infty$.

4. The design device of controller according to claim

1, characterized in that said generalized plants have a first control object model for the manipulated variables, a second control object model for the disturbance, and manipulated variable weight adjusting means for adjusting the input of manipulated variable into the first control object mode, which is provided in the former stage of said first control object model, said parameter calculating means comprises frequency response calculation means for calculating the frequency responses of said first control object model and said second control object model, and scaling matrix calculation means for calculation a scaling matrix T for determining the weighting of the manipulated variables with said manipulated variable weight adjusting means in accordance with the frequency responses of said first and second control object models so that the respective gains of said first control object model are consistent with the maximum values of the gains of said second control object model, and said controller calculation means calculates the parameters of said controller by applying said scaling matrix T to the manipulated variable weight adjusting means of said generalized plants stored in said storage means.

5. The design device of controller according to claim 4, characterized in that said scaling matrix calculation means calculates said scaling matrix T as follows:

$$T = \begin{bmatrix} T_1 & 0 & 0 & \dots & 0 \\ 0 & T_2 & 0 & \dots & 0 \\ 0 & 0 & T_3 & \dots & 0 \\ \vdots & \vdots & \vdots & \ddots & \vdots \\ 0 & 0 & 0 & \dots & T_N \end{bmatrix}$$

$$T_N = \frac{1}{L} \cdot \frac{\max(\|G_{y1w1}\|_\infty, \|G_{y1w2}\|_\infty, \dots, \|G_{y1wJ}\|_\infty)}{\|G_{y1uN}\|_\infty} \\ + \frac{1}{L} \cdot \frac{\max(\|G_{y2w1}\|_\infty, \|G_{y2w2}\|_\infty, \dots, \|G_{y2wJ}\|_\infty)}{\|G_{y2uN}\|_\infty} \\ + \dots + \frac{1}{L} \cdot \frac{\max(\|G_{yLw1}\|_\infty, \|G_{yLw2}\|_\infty, \dots, \|G_{yLwJ}\|_\infty)}{\|G_{yLuN}\|_\infty}$$

where the number of manipulated variables u is N (N is a positive integer), the number of disturbance w is J (J is a positive integer), the number of controlled variables y is L (L is a positive integer), the H_∞ norm of the transfer function of said first control object model from the N -th manipulated variable u_N to the L -th controlled variable y_L is $\|G_{yLuN}\|_\infty$, and the H_∞ norm of the transfer function of said second control object model from the J -th disturbance w_J to the L -th controlled variable y_L is $\|G_{yLwJ}\|_\infty$.

6. The design device of controller according to claim 2, characterized in that the generalized plants stored in said storage means have control variable weight adjusting means for adjusting the controlled variables inside a closed loop system consisting of said manipulated variable weight adjusting means, the control object model and the controller, and said design device has setting means for setting a weight

matrix S for determining the weighting of the controlled variables with said control variable weight adjusting means.

7. The design device of controller according to claim 4, characterized in that the generalized plants stored in said storage means have control variable weight adjusting means for adjusting the controlled variables inside a closed loop system consisting of said manipulated variable weight adjusting means, the first control object model and the controller, and said design device has setting means for setting a weight matrix S for determining the weighting of the controlled variables with said control variable weight adjusting means.

8. The design device of controller according to claim 2, characterized in that the generalized plants stored in said storage means have control variable weight adjusting means for adjusting the controlled variables in the former or latter stage of frequency sensitivity weight adjusting means for determining the set value followup characteristic of a closed loop system consisting of said manipulated variable weight adjusting means, the control object model and the controller, and said design device has setting means for setting a weight matrix S for determining the weighting of the controlled variables with said control variable weight adjusting means.

9. The design device of controller according to claim 4, characterized in that the generalized plants stored in said storage means have control variable weight adjusting

means for adjusting the controlled variables in the former or latter stage of frequency sensitivity weight adjusting means for determining the set value followup characteristic of a closed loop system consisting of said manipulated variable weight adjusting means, the first control object model and the controller, and said design device has setting means for setting a weight matrix S for determining the weighting of the controlled variables with said control variable weight adjusting means.

10 10. The design device of controller according to claim 1, characterized in that said parameter calculating means has setting means for setting the transient response characteristic of said closed loop system and frequency sensitivity weight calculation means for calculating the frequency sensitivity weight for determining the set value followup characteristic of said closed loop system in accordance with the transient response characteristic of said closed loop system, and said controller calculating means calculates the parameters of said controller by applying said frequency sensitivity weight to said generalized plants stored in said storage means.

11. The design device of controller according to claim 10, characterized in that said frequency sensitivity weight calculation unit calculates said frequency sensitivity weight in accordance with the transient response characteristic of said closed loop system, and a design index that the H_{∞} norm of the transfer function of the closed loop

system from the set value to the deviation multiplied by said frequency sensitivity weight is less than 1.

12. The design device of controller according to claim 10, characterized in that said setting means approximates the transient response characteristic of said closed loop system with a first-order lag characteristic.

13. The design device of controller according to claim 10, characterized in that said setting means approximates the transient response characteristic of said closed loop system with a second-order system characteristic.

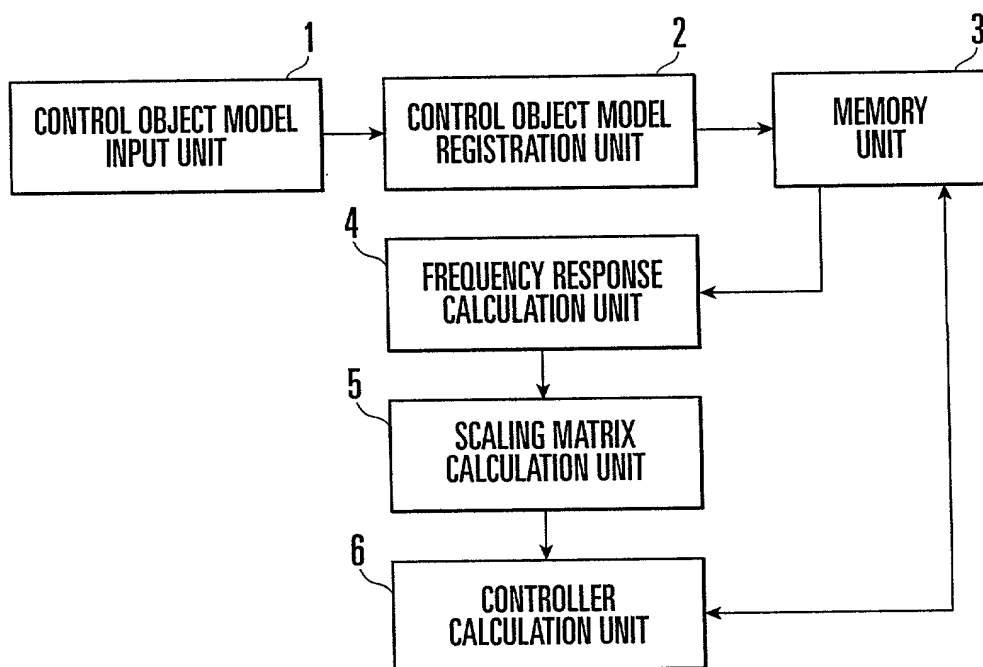


FIG. 1

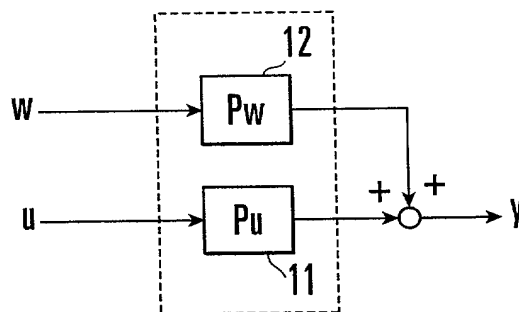


FIG. 2

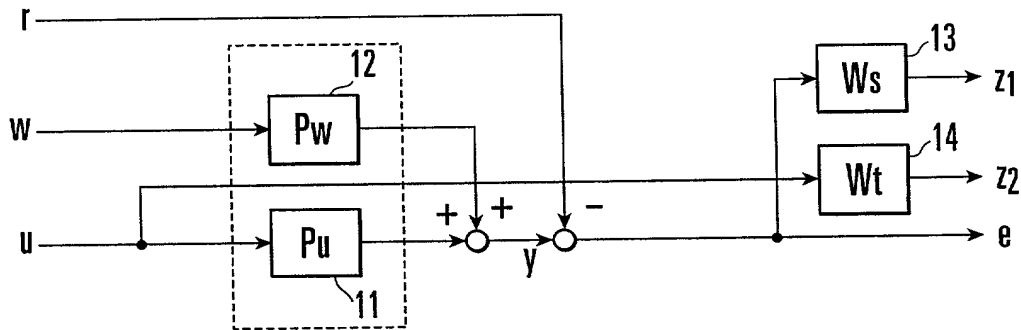


FIG. 3

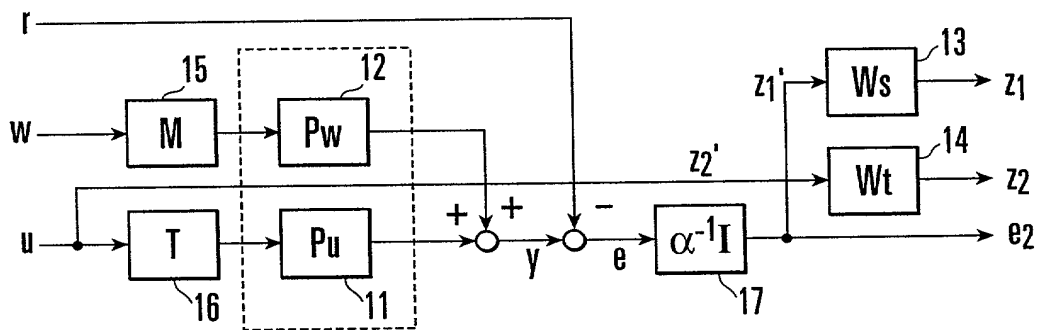


FIG. 4

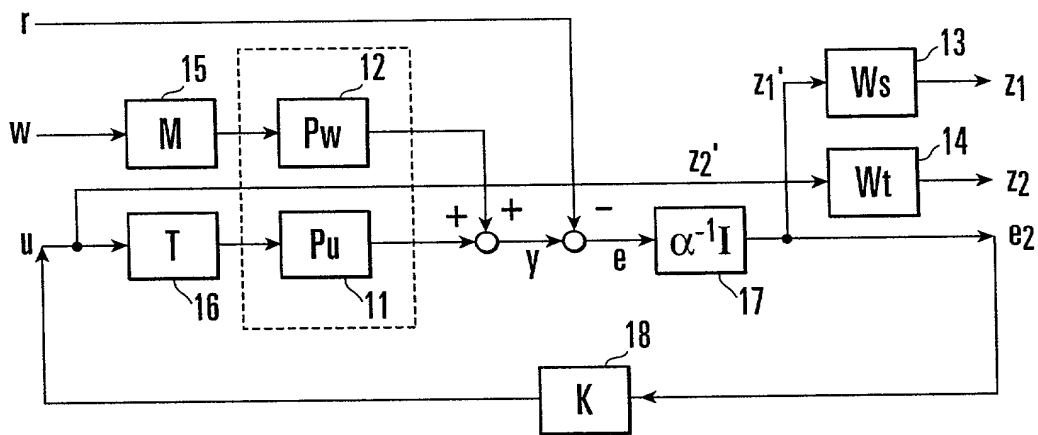


FIG. 5

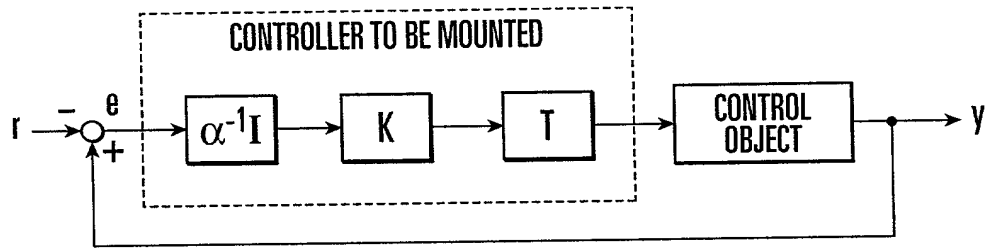


FIG. 6

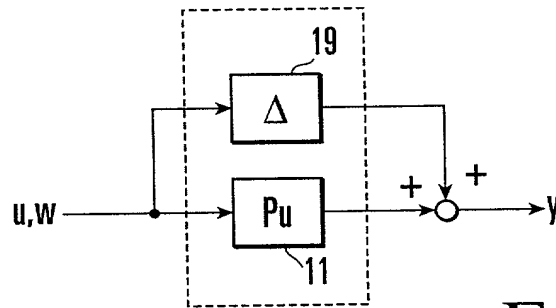


FIG. 7

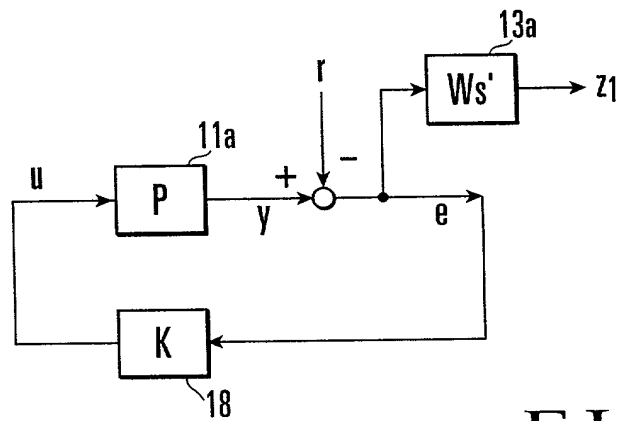


FIG. 8

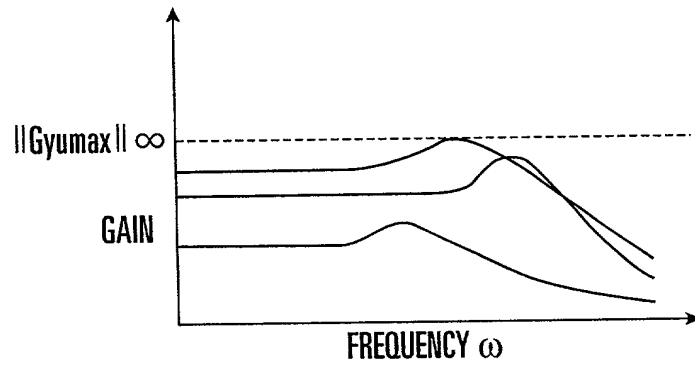


FIG.9A

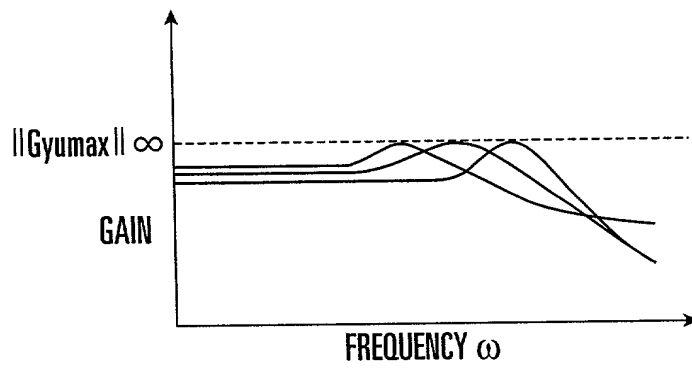


FIG.9B

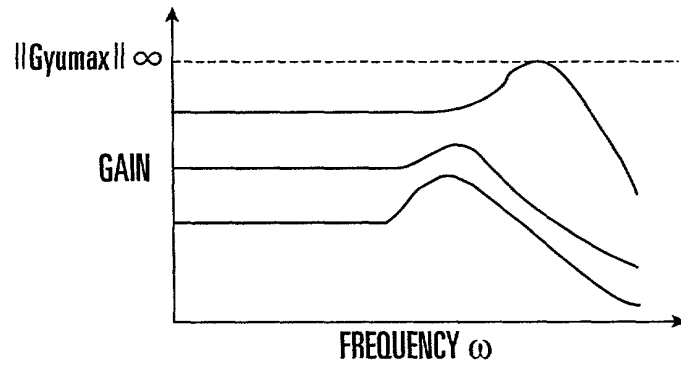


FIG. 10A

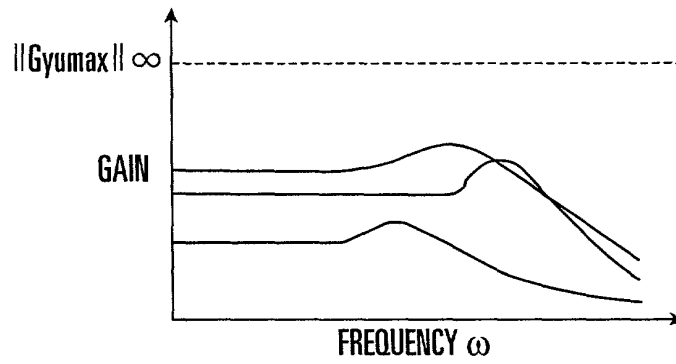


FIG. 10B

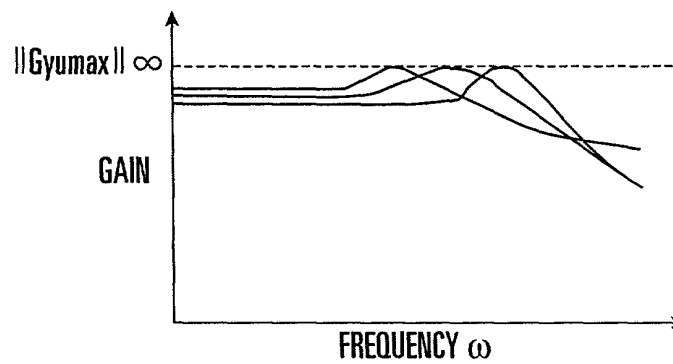
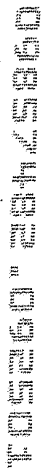
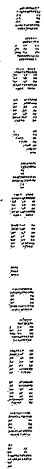


FIG. 10C



Questions and answers on the new *Code of Practice for the Management of Health and Safety at Work* are available on the HSE website at <http://www.hse.gov.uk/codeweb/>



Questions and answers on the new *Code of Practice for the Management of Health and Safety at Work* are available on the HSE website at <http://www.hse.gov.uk/codeweb/>

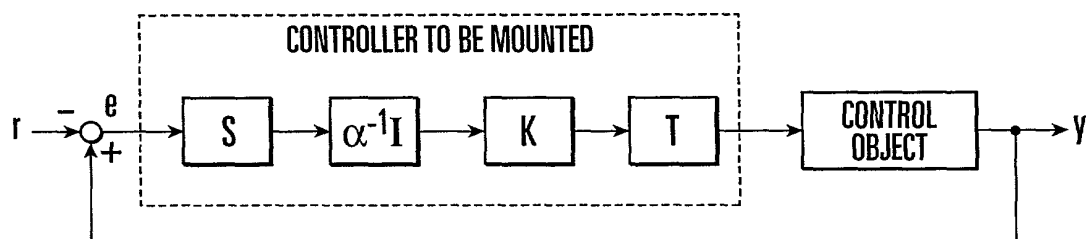


FIG. 13

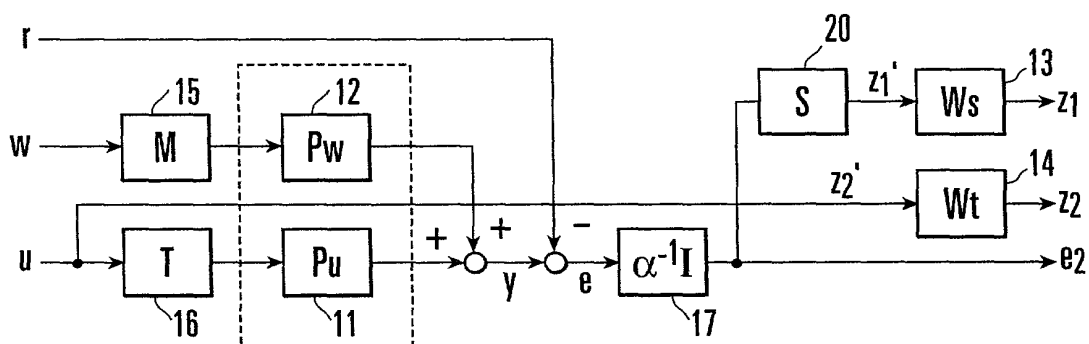


FIG. 14

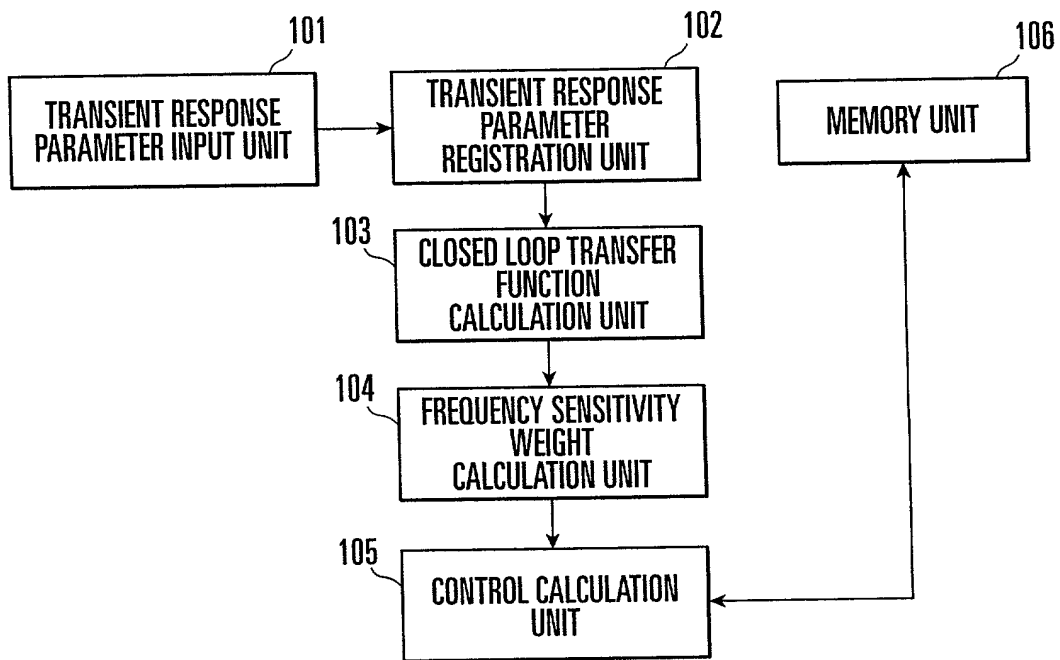


FIG. 15

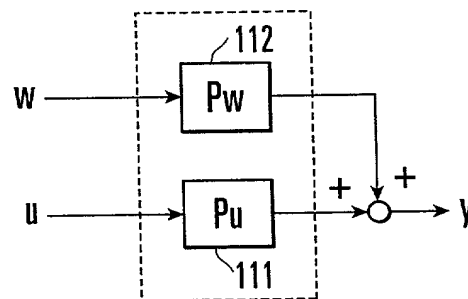


FIG. 16

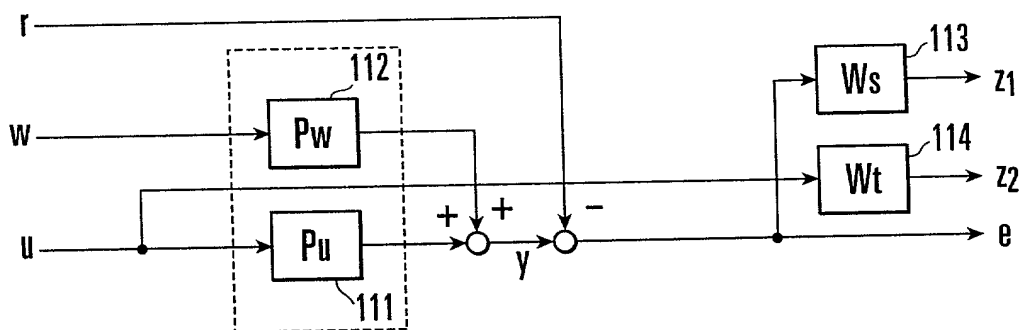


FIG. 17

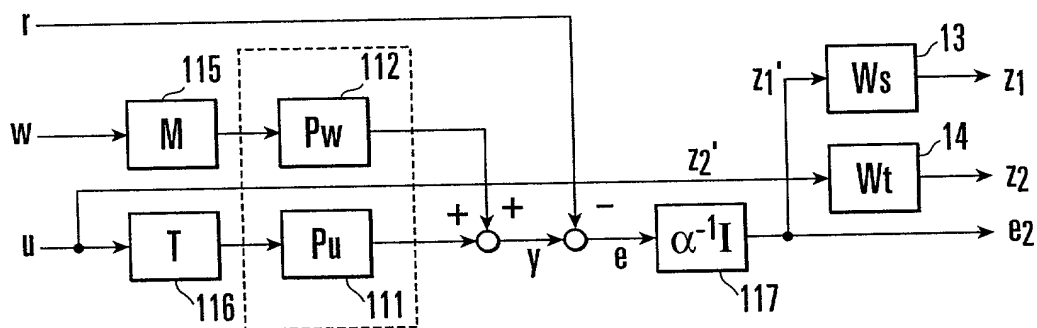


FIG. 18

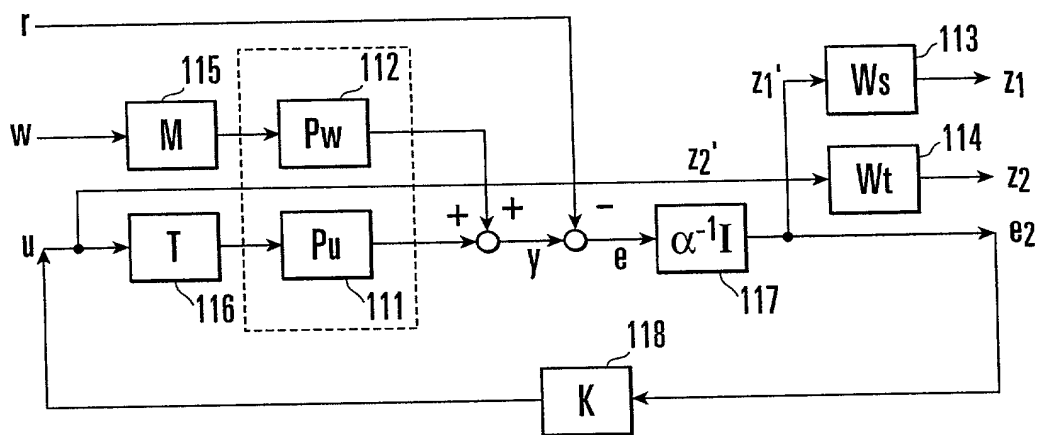


FIG. 19

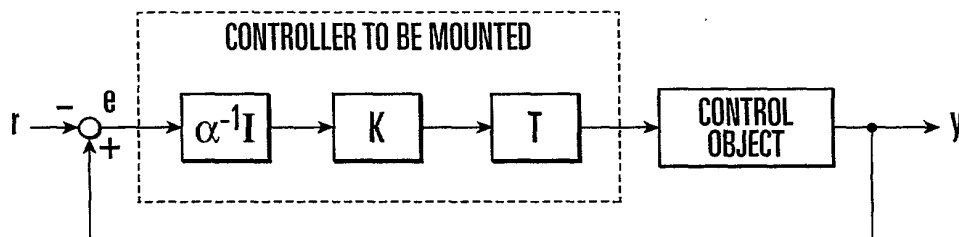


FIG. 20

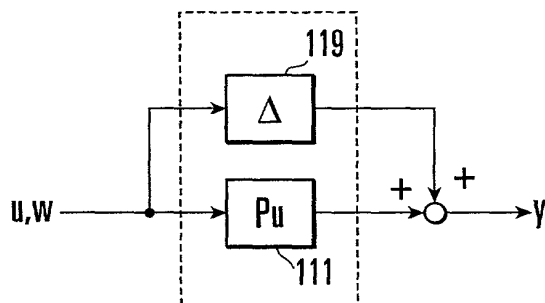


FIG. 21

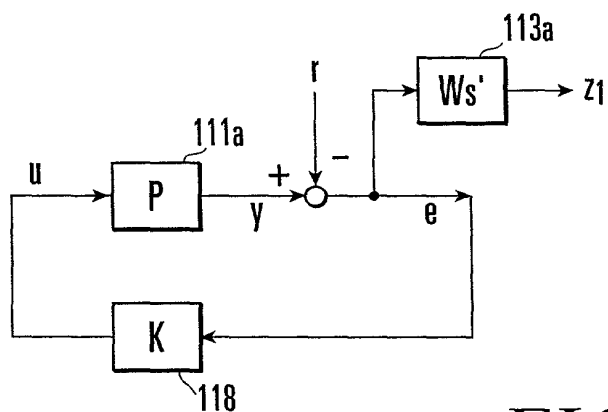


FIG. 22

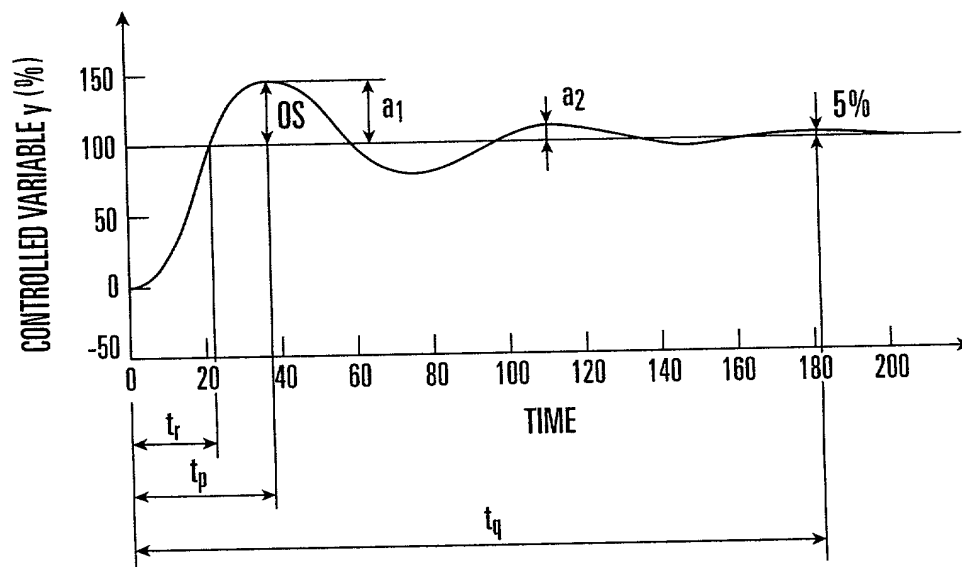


FIG.23



P14751-A

Our Ref.: _____

DECLARATION AND POWER OF ATTORNEY FOR PATENT APPLICATION

As a below named inventor, I hereby declare that:

My residence, post office address and citizenship are as stated below, next to my name,

I believe I am the original, first and sole inventor (if only one name is listed below) or an original, first and joint inventor (if plural names are listed below) of the subject matter which is claimed and for which a patent is sought on the invention entitled

Design Device of Controller

the specification of which

 x is attached hereto.
was filed on June 1, 2001 as
Application Serial No. 09/857,482
and was amended on _____
(if applicable)

I hereby state that I have reviewed and understand the contents of the above-identified specification, including the claims, as amended by any amendment referred to above. I do not know and do not believe that the same was ever known or used in the United States of America before my invention thereof, or patented or described in any printed publication in any country before my invention thereof or more than one year prior to this application, that the same was not in public use or on sale in the United States of America more than one year prior to this application, and that the invention has not been patented or made the subject of an inventor's certificate issued before the date of this application in any country foreign to the United States of America on an application filed by me or my legal representatives or assigns more than twelve months prior to this application.

I acknowledge the duty to disclose information which is material to the examination of this application in accordance with Title 37, Code of Federal Regulations, Section 1.56(a).

I hereby claim foreign priority benefits under Title 35, United States Code, Section 119, of any foreign application(s) for patent or inventor's certificate listed below and have also identified below any foreign application for patent or inventor's certificate having a filing date before that of the application on which priority is claimed:

<u>Prior Foreign Application(s)</u>			<u>Priority Claimed</u>	
<u>283978/1999</u>	<u>Japan</u>	<u>05/10/1999</u>	<u> x </u>	
(Number)	(Country)	(Day/Month/Year Filed)	Yes	No
<u>283981/1999</u>	<u>Japan</u>	<u>05/10/1999</u>	<u> x </u>	
(Number)	(Country)	(Day/Month/Year Filed)	Yes	No
<u>PCT/JP00/06898</u>	<u>WIPO</u>	<u>04/10/2000</u>	<u> x </u>	
(Number)	(Country)	(Day/Month/Year Filed)	Yes	No
_____	_____	_____	Yes	No
(Number)	(Country)	(Day/Month/Year Filed)	Yes	No
_____	_____	_____	Yes	No
(Number)	(Country)	(Day/Month/Year Filed)	Yes	No
_____	_____	_____	Yes	No
(Number)	(Country)	(Day/Month/Year Filed)	Yes	No

I hereby claim the benefit under Title 35, United States Code, Section 120 of any United States application(s) listed below and, insofar as the subject matter of each of the claims of this application is not disclosed in the prior United States application in the manner provided by the first paragraph of Title 35, United States Code, Section 112, I acknowledge the duty to disclose material information as defined in Title 37, Code of Federal Regulations, Section 1.56(a) which occurred between the filing date of the prior application and the national or PCT international filing date of this application:

(Application Serial No.)	(Filing Date)	(Status -- patented, pending, abandoned)
(Application Serial No.)	(Filing Date)	(Status -- patented, pending, abandoned)
(Application Serial No.)	(Filing Date)	(Status -- patented, pending, abandoned)

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I hereby declare that all statements made herein of my own knowledge are true and that all statements made on information and belief are believed to be true; and further that these statements were made with the knowledge that willful false statements and the like so made are punishable by fine or imprisonment, or both, under Section 1001 of Title 18 of the United States Code and that such willful false statements may jeopardize the validity of the application or any patent issued thereon.

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